

APPLICATION OF HOLOGRAPHIC INTERFEROMETRY  
TO THE INTERIOR BALLISTIC FLOW FIELD IN  
THE BARREL OF A TWENTY MILLIMETER CANNON

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# THESIS

APPLICATION OF HOLOGRAPHIC INTERFEROMETRY  
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THE BARREL OF A TWENTY MILLIMETER CANNON

by

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September 1976

Thesis Advisor:

D. J. Collins

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to the Interior Ballistic Flow Field in  
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by

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### ABSTRACT

The technique of holographic interferometry was applied to the study of gas core characteristics in the barrel of a 20mm cannon. Using standard hydrodynamic equations theoretical predictions were calculated. Holographic interferograms were made of the associated flow field near the projectile during firing. Reconstruction of the wavefront provided the necessary means of comparing experimental results with the theoretical values obtained.



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## LIST OF SYMBOLS

<u>SYMBOL</u>	<u>DEFINITION</u>
A	Cross-section area
C	Constant specifying thickness of shock region
E	Specific internal energy
j	Mass point number
M	Mass
P	Pressure
q	Artificial viscosity
t	Time
u	Velocity
V	Specific Volume
X	Eulerian Position
$\rho$	Density



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## I. INTRODUCTION

For many years the field of theoretical interior ballistics was almost entirely confined to a single problem: given the characteristics of shot, charge, and gun, to calculate the muzzle velocity and peak pressure. (Ref. 1)

With the discovery of the laser and its application to holography, more interesting information can be obtained. It is possible to make a hologram of the projectile and its flow field, then reconstruct the image with exact detail.

Having a thorough knowledge of the physical characteristics of the internal gas flow field is essential in ballistic design. Although thermochemical constants for the products of combustion during actual gun firing are not well known, it is assumed that the gas and the solid grains move together as a homogeneous mixture. If this is true, then the conclusions of the Lagrange hypothesis are applicable to the interior ballistics of a gun.

The motion of the projectile creates a system of rarefaction waves in the breech, with relaxation occurring through the mechanisms of stress transfer in the bed and in the propellant gas. The dual wave system will accelerate the gas and the particles in the direction of the projectile



motion at the expense of stored internal energy. The more volatile gas will follow the projectile more readily than the particles. With progressive motion of the projectile, the initial unsteady flow may be expected to damp out and, as the motion evolves, to assume the quasi-equilibrium character of the Lagrange solution. This is a flow in which the mixture has uniform density, a linear velocity distribution and a quadratic pressure distribution. Eventually, the propellant is consumed entirely. Subsequent motion involves only the propulsion of the projectile by the reservoir of energetic gas. (Ref. 2)

It is the purpose of this investigation to utilize laser techniques and observe this flow field responsible for propelling the projectile as it transits through the barrel of a gun.



## II. HOLOGRAPHIC INTERFEROMETRY

Holography is a process which is similar to photography in certain respects, but is nonetheless fundamentally different. Photography provides a method of recording the two-dimensional irradiance distribution of an image. Generally speaking each "scene" consists of a large number of reflecting or radiating points of light. The waves from each of these elementary points all contribute to a complete wave which we call the "object wave." This complex wave is transformed by the optical lens in such a way that it forms an image of the radiating object. It is this image which is recorded on the photographic emulsion.

Holography is quite different. With holography one actually records the object wave itself. This wave is recorded in such a way that subsequent illumination of the record serves to reconstruct the original object wave even in the absence of the object. A visual observation of this reconstructed wavefront then yields a view of the object or scene which is practically indiscernible from the original.

The method of recording the object wave is as follows. One starts with a single monochromatic beam of light which



has originated from a very small source. The requirement of coherence means that the light should be capable of displaying interference effects that are stable in time. This single beam of light is then split into two components, one of which is directed toward the object or scene; the other is directed to a suitable recording medium. The component beam that is directed to the object is scattered, or diffracted, by that object. This scattered wave constitutes the object wave, which now is directed to the recording medium. The wave that proceeds directly to the recording medium is the reference wave. Since the object and reference waves are mutually coherent, they will form a stable interference pattern when they meet on the recording medium. The detailed permanent record of this interference pattern on the recording medium is called the "hologram." This method is illustrated in Figure 1. When the hologram is illuminated with a beam of light which is similar to the original reference wave used to record the hologram, light will be transmitted only through the clear areas, resulting in a complex transmitted wave. Because of the recorded interference fringes, this wave conveniently divides into three separate components, one of which exactly duplicates the original object wave. By viewing





this reconstructed wavefront, one sees an exact replica of the original object. Three-dimensional images of opaque objects may be reconstructed and photographed from different viewing angles using a single hologram.

The above description of holography can be represented mathematically as follows:

Let  $\bar{E} = \bar{O} + \bar{R}$  2.1

Where  $O$  represents the object or scene beam

$R$  represents the reference beam

Then  $E^2 = O^2 + R^2 + 2\langle \bar{O} \cdot \bar{R} \rangle$  2.2

Taking the time average:

$$\langle \bar{E}^2 \rangle = I = I_O + I_R + 2\langle \bar{O} \cdot \bar{R} \rangle \quad 2.3$$

The term  $2\langle \bar{O} \cdot \bar{R} \rangle$  in equation 2.3 is the interference term. Without interference the intensity of the two beams are merely additive. With the utilization of monochromatic light derived from a single ideal source, interference is always possible.

Uncorrelated light beams, as from two different light sources, are uncorrelated and are called incoherent. Coherent radiation produces interference effects. The superposition of incoherent radiation yields the addition of the intensities of the object and reference beams.



The interference term contains both amplitude and phase information. Consider two waves such that:

$$\bar{O} \cdot \bar{R} = \frac{1}{2} (\bar{O} e^{-i\omega t} + \bar{O}^* e^{i\omega t}) (\bar{R} e^{-i\omega t} + \bar{R}^* e^{i\omega t}) \quad 2.4$$

Then

$$\bar{O} \cdot \bar{R} = \frac{1}{2} \left\{ \bar{O} \cdot \bar{R} e^{-2i\omega t} + \bar{O}^* \bar{R}^* e^{2i\omega t} + \bar{O} \cdot \bar{R}^* + \bar{O}^* \cdot \bar{R} \right\} \quad 2.5$$

$$2 \langle \bar{O} \cdot \bar{R} \rangle = \frac{1}{2} (\bar{O} \cdot \bar{R}^* + \bar{O}^* \cdot \bar{R}) \quad 2.6$$

If  $O_1 = O_1 e^{ig_1}$  etc. and  $R_1 = r_1 e^{ih_1}$

$$\begin{aligned} 2 \langle \bar{O}_1 \cdot \bar{R}_2 \rangle &= O_1 r_1 \cos(g_1 - h_1) + O_2 r_2 \cos(g_2 - h_2) \\ &+ O_3 r_3 \cos(g_3 - h_3) \end{aligned} \quad 2.7$$

Thus the interference term contains both amplitude and phase information. From equation 2.6 it is evident that interference occurs only when light beams of the same polarity interact with one another.

The complete interference equation is:

$$I = \langle \bar{E}^2 \rangle + I_R + I_O + R \cdot O^* + O \cdot R^* \quad 2.8$$

where  $\langle R \cdot R^* \rangle = I_R$

and  $\langle O \cdot O^* \rangle = I_O$

The reconstruction process can also be described with equation 2.8. The amplitude transmittance of the hologram



is assumed to be proportional to the intensity

$$t(x) + KI \tag{2.9}$$

On reconstruction with the reference beam R, the following is obtained:

$$R \cdot KI = R(I_R + I_0) + R \cdot R \cdot O^* + R \cdot R^* \cdot O \tag{2.10}$$

The last term in equation 2.10 is the reconstructed object beam.

A primary consideration in the technique of holographic interferometry of flow fields is the source of coherent light. The Q-switched ruby laser has proved to be an excellent light source for these applications. It provides the high power necessary to expose the plate in a time frame suitable for freezing the motion of the flow field.

The wavelength of this laser is  $6943 \overset{\circ}{\text{A}}$ , which is compatible with AGFA-GEVAERT 10E75 holographic film plates. (Ref. 3)



### III. EXPERIMENTAL LAYOUT

#### A. GENERAL PHYSICAL ARRANGEMENT

The experiment was conducted at the Naval Postgraduate School Rocket Laboratory. The laboratory contained four test cells measuring 12' X 17' with reinforced concrete walls 12" thick. A control room with observation windows was located directly behind the test cells.

The 20mm cannon was mounted horizontally on a rocket test stand. Two steel mounts were used to secure the barrel in place at a height of 6.5 inches from barrel center line to the top of the test stand.

Two large wooden tables were constructed and placed parallel to and on either side of the test stand. The tables provided a platform for the optical equipment necessary to obtain holograms. The tables were rigidly fastened together; however, they were completely isolated from the test stand to ensure stability during cannon operation. Furthermore, plywood boxes were constructed to fit over the tables and completely house the optical equipment. The plywood boxes not only acted as protection for the equipment but also acted as a light shield for the





holographic process. The tops of the plywood boxes were hinged in order to allow easy access to the optical equipment.

The muzzle of the cannon faced a bullet trap located 13 feet outside the test cell. The bullet trap contained an 18" X 18" X 1½" armored plate, tilted 45° from the path of the projectile, and a sand trap measuring 5' X 5' X 2½'.

Upon bullet impact, the plate shattered the projectile and deflected the fragments into the sandtrap. In order to provide additional safety, the entire sandtrap was housed inside a steel turret for a 5" gun mount measuring approximately 15' X 20' X 10'.

An electrical firing mechanism was placed at the breech end of the cannon. The firing sequence was directed from the control room.

A light shield was provided to cover the observation window during placement and removal of the holographic plates.

The ruby laser and its components were fixed in position in a test cell adjacent to the cell housing the 20mm cannon. The purpose of this placement was necessary not only for space consideration but mostly for protection of the instrument. A specially constructed table provided support for the laser rail system. The laser was placed normal to the



wall separating the two cells. (Figure 2) A 2-inch hole was drilled through the concrete wall to allow beam passage. A water source for the laser head and output etalon cooling system was incorporated within the test cell. The laser was equipped with a remote control making it possible to fire either from the test cell or the control room. (See Figure 3)

## B. BARREL INSTRUMENTATION

For viewing the projectile inside the cannon a .817" diameter hole was drilled completely through the barrel 4.5" from the muzzle. In order to preserve the integrity of the barrel, projectile and flow field, plexiglass windows were designed to seal the port and provide observation inside the barrel. (See Figure 4)

The windows were milled from optical quality 3/4" plexiglass. Two windows were pressure tested in a simulated barrel to 6000 PSI, thus ensuring strength capabilities necessary to withstand internal pressures present. (See Figure 5)

Figure 6 shows the design consideration met for mounting the windows in the barrel. Figure 7 shows the actual barrel with window and with collar.



Figure 8 shows the collar device used to secure the windows in the barrel.

A Kistler 607A pressure transducer was installed 5.5 inches from the breech end of the barrel. This location was just ahead of the tip of the projectile prior to firing. The signal from the transducer was relayed to a Kistler model 504 universal charge amplifier located in the control room. The signal from the charge amplifier was passed to a Textronix 549 storage oscilloscope. The oscilloscope allowed the signal to be time delayed by a predetermined amount and then amplified to +30 volts, which in turn was used to trigger the xenon flash tube of the Korad K-1 pulsed ruby laser.

A Kistler 603H pressure transducer was located 2.5 inches aft of the observation ports. The signal from the transducer was relayed to a Kistler model 504A universal charge amplifier located in the control room. The signal from the charge amplifier was passed to a Hewlett Packard Model 214A pulse generator where it could be delayed and amplified. The resulting pulse was used to energize the Pockel cells of the Korad K-1 pulsed ruby laser.

The muzzle velocity was measured by the use of two Oehler Model 55 ballistic velocity screens. The screens



were mounted 4 feet apart and placed 81.25 inches from the muzzle of the cannon. As the projectile passed through each screen a 12-volt pulse with an adjustable 2-8 milli-second pulse length was produced and relayed to an Oehler Model 21 chronograph. The two pulses provided a start and stop for the chronograph. Tables of velocities were provided for known screen separation. (See Figure 9)

### C. OPTICAL SYSTEM

Figure 10 shows the optical layout used to accomplish the holography. The Korad K-1 pulsed ruby laser was used for the holography process. By utilizing the laser system in the Q-switch mode of operation, high power single transverse mode output could be obtained. A Pockel cell was used to achieve the Q-spilling required for peak output power.

When operating the Korad K-1 pulse ruby laser in the  $tem_{00}$  mode a peak power of 2.5 megawatts with pulse energy of .050 joules over a pulse width of 20 nanoseconds can be realized. The output beam measured approximately 2mm in diameter at a wavelength of  $6943\overset{\circ}{\text{A}}$  with a coherence length that exceeds one meter. Figure 3 shows a photographic view of the laser installation.





The laser beam passes through a 2-inch hole in the concrete wall then through another 2-inch hole in the plywood boxes where it first contacts a narrow-band filter which removes the undesired light from the xenon flash tube. The beam then strikes a 2-inch round beam splitter where it is divided into two wave fronts, a scene beam and a reference beam. The intensity of the reference beam is about twice that of the scene beam.

The scene beam is directed along the centerline of a 2.5 meter optical bench where prior to striking mirror #1 it passes through a collimating lens, double concave lens and another collimating lens.

The lens arrangement was designed to allow the scene beam to be expanded to a diameter compatible with the hole drilled through the barrel of the 20mm cannon.

Mirror #1 directed the beam through the windows in the 20mm cannon and onto mirror #2. In order to accomplish this, 3-inch holes were cut in the plywood boxes to permit the beam to pass, allowing enough tolerance for adjustment to ensure that the beam passed through the windows normal to the cannon's axes. Furthermore, mirror #1 was secured to a gimbal mount which allowed a fine adjustment to be made in the horizontal and vertical axes.



Mirror #2 directed the scene beam down the centerline of a 1.5 meter optical bench where a second narrow-band filter was located to remove the unwanted flash from the cannon blast. The beam then proceeds through an expanding collimating lens to mirror #3 where it is directed to the holographic plate. The location of the expanding collimating lens makes it possible to enlarge the scene beam from test section (window size) diameter to a diameter of approximately 4-inches.

After passing the beam splitter the reference beam proceeded to mirror #4 on a 2.0 meter optical bench. The physical arrangement allowed the reference beam to be adjusted to the same length as the scene beam. Mirror #5 directs the beam through two series of expanding--collimating lenses which enlarged the reference beam to approximately 4-inches in diameter at the holographic plate.

Throughout the entire system the optical benches were bolted to the tables on specially designed cross feet which allowed the system to be leveled by adjustment knobs located at each crossfoot. The alignment procedure was greatly simplified by the use of mirrors which contained screw type adjustments for vernier-scale movement about the horizontal and vertical axes. In addition, all the optical components



could be easily positioned along the optical bench. Figure 11 shows the actual optical layout with one plywood box removed to show the arrangement.

The alignment of the system was accomplished by the use of a coherent radiation 3-milliwatt helium-neon continuous wave laser. This laser was mounted on a stand which was placed perpendicular to the axis of the ruby laser cavity. By firing the ruby laser on an exposed polaroid paper a "spot" could be obtained which was used in the alignment process. By placing a mirror at a  $45^{\circ}$  angle in the ruby laser cavity, the CW beam could be directed through the cavity and centered on the "spot." This centered beam would then coincide with the ruby laser beam and the optical system could be accurately aligned.



#### IV. FIRING SEQUENCE

All the electrical equipment was turned on to allow the required warm-up time while the test section and optical system were being prepared and aligned. The barrel test section assembly required particular care when installing the plexiglass windows, to ensure that the faces were parallel to the center line of the cannon and normal to the laser beam's path.

After the system was aligned, all electrical equipment was checked for proper settings and all timers zeroed. The opening into the plywood box containing the holographic plate was covered and the alignment mirror removed. The test cell was closed and a holographic plate was placed in its holder. The test cell door was raised to a level just above the muzzle of the 20mm cannon. At this time the cannon was loaded.

The individual who was loading the cannon and connecting the firing mechanism carried with him a safety key which broke the firing circuit at the control panel to prevent accidental firing prior to his clearing the test area. Following loading, the opening into the plywood box





containing the hologram was uncovered and control was then commenced from the control room. All electrical equipment was scanned and the warning horn sounded to alert personnel of the impending shot. The firing sequence was then initiated. A schematic of this sequence is shown in Figure 12.

The charge switch for the laser capacitor was activated. While the capacitor bank was charging, the safety key was installed in the fire control panel and power supplied to the firing mechanism. When the laser ready light illuminated the firing mechanism, capacitors were charged and the cannon fired. Figure 13 shows a view of the control room and monitoring equipment.

The firing process was observed through the observation window. A light shield was placed against the window after firing to protect the hologram from unwanted illumination.

Actual bullet movement was used to fire the laser. On initial firing, a pulse from the Kistler transducer located at the breech was passed to the Textronix 549 storage oscilloscope, where it was delayed and amplified, then used to trigger the xenon flash tube of the Korad K-1 pulsed ruby laser. Considering that the pumping time for the laser is approximately 1000 microseconds and that



approximately 1500 microseconds are needed for projectile travel to the test area, 500 microseconds was used for the pulse delay.

When the projectile reached the second Kistler transducer another pulse was initiated that was relayed to a Kistler model 504A charge amplifier then to a Hewlett Packard Model 214A pulse generator. The pulse generator provided the voltage necessary to trigger the Pockel cell of the Korad K-1 pulsed ruby laser. This unit allowed for a variable signal delay which was used to adjust the time interval for laser firing. Two Monsanto Model 101B timers were incorporated into the system at various locations to provide checks on intervals of interest. Also a Korad KD energy monitor was employed to check the actual laser firing interval.

After firing, the test cell was closed and the hologram removed for processing. The armor plate was inspected for integrity and repositioned if necessary. The 20mm cannon was unloaded and the windows removed and examined for damage.



## V. HOLOGRAPHIC FILM AND PROCESSING TECHNIQUE

The Korad K-1 pulsed ruby laser delivered a beam at a wavelength of  $6943\overset{\circ}{\text{A}}$ . In order to minimize the effects of extraneous light leakage into the system a photographic emulsion with narrow band sensitivity centered in this region was selected. Agfa-Gevaert 10E75 holographic plates were found to be the most suitable for this purpose. This film has a resolution capability of 2800 lines per mm. For holograms produced with  $6943\overset{\circ}{\text{A}}$  light this is nearly the required maximum resolution. Reference 4 gives a spectral sensitivity curve for the emulsion.

Following exposure to the laser light the hologram plate was removed from its holder and placed in a closed container and taken to a dark room for development. The initial processing required a five minute bath in kodak D-19 developer. The entire five minute bath was completed in total darkness. Then the plate was rinsed and placed for five minutes in a standard fixer. After 30 seconds in the fixer it was permissible, although not necessary, to turn on green photographic lights in the dark room. From the fixer the plate was washed in water for five minutes and then allowed to air dry. During the entire development



procedure, when it became necessary to touch the hologram it was handled by the edges in an attempt to keep the hologram clear of unwanted finger markings.

When using the 20-nanosecond ruby pulse, it was not possible to control exposure time. Therefore, to ensure the desired intensity, a combination of suitable neutral density filters were placed in the beam paths.





## VI. RECONSTRUCTION

To reconstruct the holograms a 15-milliwatt Spectra Physics continuous wave, helium-neon laser was used for the reconstructing wave. A Spectra Physics collimator was fastened to the laser, causing the beam to be expanded to approximately four inches in diameter. The beam was directed to pass through the hologram as outlined in Part I. The converging real image was then photographed with a single reflex polaroid camera using type 55 positive-negative film. This film has a resolution capability of 150-165 lines per mm negative, 14-17 lines per mm positive, thus providing excellent results. The reconstruction process is illustrated in Figure 14. The negatives were further processed at the Naval Postgraduate School photo lab, from which prints were produced.



## VII. COMPUTER PROGRAM FOR PREDICTIONS OF FLOW PARAMETERS

The computer program used to predict the velocity of the projectile, pressure and total energy of the flow field was an adaption of a program developed at the Naval Ordnance Laboratory. The program was originally concerned with the analysis of hypervelocity model launchers (Ref. 5). The method of analysis used was essentially a one-dimensional, Lagrangian scheme where the field was divided into six regions each of which in turn was divided into zones. At the interface of each zone mass points were inserted. Each mass was considered to consist of one-half of the mass of the adjacent zone. The hydrodynamic equations, in finite difference form, were then applied to each mass point during the particular interval of interest. The method employed was the "q" method of Von-Neumann and Richtmyer (Ref. 6 and 7).

The following equations were used for this method:

Isentropic flow energy equation;

$$\frac{\partial E}{\partial t} = -(P+q) \frac{\partial v}{\partial t}$$

Equation of motion;

$$\frac{\partial u}{\partial t} = - \frac{\partial (P+q)}{\partial x} \frac{1}{M} A(x)$$



Equation of state;

$$P = P(E, v)$$

$$M = \int^X (X)A(X) dx$$

with

$$\left\{ \begin{array}{ll} \frac{C_0^2}{v} \frac{\partial u}{\partial y} & , \quad \frac{\partial u}{\partial y} < 0 \\ 0 & , \quad \frac{\partial u}{\partial y} \geq 0 \end{array} \right.$$

The artificial viscosity term "q" was added to the pressure term in the energy and motion equations in order to spread variable changes created by the shock over a finite region. This allows the equation variables to be considered continuous across the shock. The constant  $C_0$  permits adjustment of the shock "thickness."

The equations were written in finite difference form with initial values of  $E_0$ ,  $P_0$ , and  $V_0$  being provided for each region. In order to maintain stability during the process, a new time increment was calculated for each cycle.

During each cycle the pressure was calculated at each mass point using the equation of state and energy. The differential in pressure between mass points was then applied to the equation of motion to determine the acceleration and velocity of each mass point.



For each region it is necessary to input the initial temperature, pressure, molecular weight and a geometrical description.

The program was written in FORTRAN. A listing of the program and the input is given in Appendix A.





## VIII. HOLOGRAPHIC RESULTS

Initially the first few holograms obtained appeared to be in the region several centimeters in front of the projectile. However, when further experimental studies did not give the desired results, an investigation was initiated to examine the laser system. It was then discovered that a short circuit had occurred between the plate and cathode of the large thyatron of the Korad power supply. This short circuit would occur approximately 8 minutes following the application of power. This malfunction caused a firing pulse to be continually delivered to the Pockel cell; thus, nearly two-thirds of the seventy-five test firings resulted in holograms in which the laser had fired from 50 to 200 microseconds early. To further compound the problem the Korad KD energy monitor was not available to confirm actual laser firing.

With the incorporation of the energy monitor into the system, and careful monitoring of the power supply, several good holograms were obtained. Figure 15 shows a series of compression waves approximately 2 cm in front of the projectile. Figure 16 shows these same type of waves



approximately 1 cm in front of the projectile. A traveling bow wave can be seen in Figure 17. It is believed that this wave is approximately 3 mm in front of the projectile.

Due to time consideration allowed for this study, the area just behind the projectile was not captured; however, Figure 18 shows a hologram obtained approximately 30 microseconds following projectile passage through the test area. The effects of powder blast not only etch the plexiglass windows but also leave a carbon deposit over the inner faces, resulting in a clouded view of the test area. Further investigations will determine if this powder blast is directly behind the projectile or if there are several microseconds delay between the gas particles and the projectile.



## IX. COMPARISON OF ANALYTICAL AND EXPERIMENTAL RESULTS

Analytical results were obtained previously by Robert G. Bettinger (Reference 8) during his work concerning gas core characteristics in the muzzle environment of the 20mm cannon.

Figures 19 and 20 are outputs obtained by Bettinger. Figure 19 summarizes the major input data and initial conditions required, and demonstrates the output format used for representing these data. As shown in Figure 19, a printout was obtained every 0.2 milliseconds. Figure 20 illustrates the output obtained just as the projectile exits the barrel; at this time a muzzle velocity of 1064 meters per second was obtained.

It must be emphasized that the program (Reference 5) does not take into consideration the effects of frictional forces on the projectile. Therefore, in order to obtain a more realistic solution either the program must be modified or the powder parameters altered to account for this constraint. Figures 19 and 20 resulted from the latter choice.

In order to verify these results it was necessary to analyze the powder used to propel the 20mm projectile.



The type powder used in the 20mm cartridge was WC870 with a charge weight of 590 grains. WC870 is a sphere of .305" average grain diameter, with a specific gravity of 1.56 grams/cc. A representative composite is:

Nitrocellulose (13.15%N)	=	81.49%
Nitroglycerine	=	10.0 %
Dibutylphthalate	=	5.5 %
Diphenylamine	=	1.0 %
CaCO <sub>3</sub>	=	0.1 %
AsH	=	0.5 %
Graphite	=	0.15%
Na <sub>2</sub> SO <sub>4</sub>	=	0.16%
K <sub>2</sub> SO <sub>4</sub>	=	0.75%
SNO <sub>2</sub>	=	0.75%
Ethyl Acetate	=	0.10%
H <sub>2</sub> O	=	0.80%

The percentages are given of the dry weight, so that the sum of the ingredients up to the last two constituents is 100%.

The average thermochemical properties of this composition are (by Hirschfelder's approximation, reference 1) as follows:

T <sub>0</sub>	=	2856°K
n	=	0.04218 grams/mol
γ	=	1.2394
F	=	335068 ft-lbs/md
b	=	0.943 cc/gram

The molecular weight of the constituents can be found directly except for nitrocellulose. The nitrocellulose in propellant compositions varies in its nitrogen content. The cellulose molecule is a large one but, for present





purposes, it can be written  $C_6H_7O_2(OH)_3$ . On nitration, X(OH) groups are replaced by  $(ONO_2)$  groups, the value of X depending on the nitrogen content. The resulting compound is  $C_6H_7O_2(OH)_{3-X}(ONO_2)_X$ . The molecular weight is easily found to be  $(162.14 + 45X)$  and, if Y is the percentage nitrogen content,  $Y = \frac{1400.8X}{162.14 + 45X}$ . This gives  $X = \frac{162.14Y}{1400.8 - 45Y}$ . Thus for a given nitrogen content Y and X can be calculated and the atomic composition found from:

$$C = \frac{6}{162.14 + 45X} \quad H = \frac{10-X}{162.14 + 45X} \quad N = \frac{Y}{1400.8} \quad O = \frac{5 + 2X}{162.14 + 45X}$$

The heats of formation of the solid propellant can be calculated as outlined in Reference 10.

Inputting the exact values into the computer program resulted in a value of approximately 1463 M/sec. Assuming a projectile drag coefficient of 0.28 (Reference 9), this gives a muzzle velocity of 1036 meters per second which is in excellent agreement with Bettinger's theoretical results.

Furthermore, the maximum possible muzzle velocity (Reference 1) may be calculated from the following:

$$V_m = \frac{2}{\gamma - 1} (RT_0)^{\frac{1}{2}}$$

Using this equation a value of 1097 meters per second is



obtained. The projectile velocity was measured during each firing, and a range of 1020 to 1060 meters per second was obtained.

These values are in excellent agreement with the computer program.



## X. SUMMARY AND RECOMMENDATIONS

A considerable amount of difficulty was experienced while attempting to capture the projectile in the test area. Considering the velocity and length of the projectile, passage through the test area occurs within approximately 80 microseconds. Furthermore, considering just the base of the projectile, a time interval of approximately 20 microseconds would result in complete passage of the base of the projectile through the test area. Thus, timing of the laser firing with projectile firing is indeed quite critical.

Referring to Figure 21, it can be seen that the velocity of the projectile approaches a constant value at a distance of approximately 90 cm from the breech of the barrel. It was this fact that prompted the barrel modification to incorporate the pressure transducer near the test area as outlined in Part III Section B. By controlling the firing of the Pockel cell with this transducer, more consistent results were expected.

Theoretically, if the pressure transducer responded instantaneously to the passage of the gas ring of the projectile, the signal produced could be used to pulse the



Pockel cell of the laser just as the nose of the projectile entered the test area.

Unfortunately, 0.5 volts was required to trigger the Hewlett Packard Model 214A pulse generator, while the Monsanto timers responded immediately to projectile passage. Referring to the pressure trace obtained from the pressure transducer (Figure 22), approximately 100 microseconds could pass before the required 0.5 volts was obtained.

In an attempt to confirm the actual passage of the projectile through the test area the pressure transducer was replaced by a temporary contact switch. This switch could only be triggered by actual contact with the gas ring of the projectile. The test confirmed the correct timing of the projectile, agreeing with the results obtained with the pressure transducer as far as the Monsanto timers were concerned.

Due to the fact that most pulse generators require at least 0.5 volts input as a trigger and that the pressure transducer used takes anywhere from 0-100 microseconds to reach 0.5 volts, it is felt that a more positive device must be used to sense the actual position of the projectile. This could be accomplished with a contact switch designed specifically for this purpose.





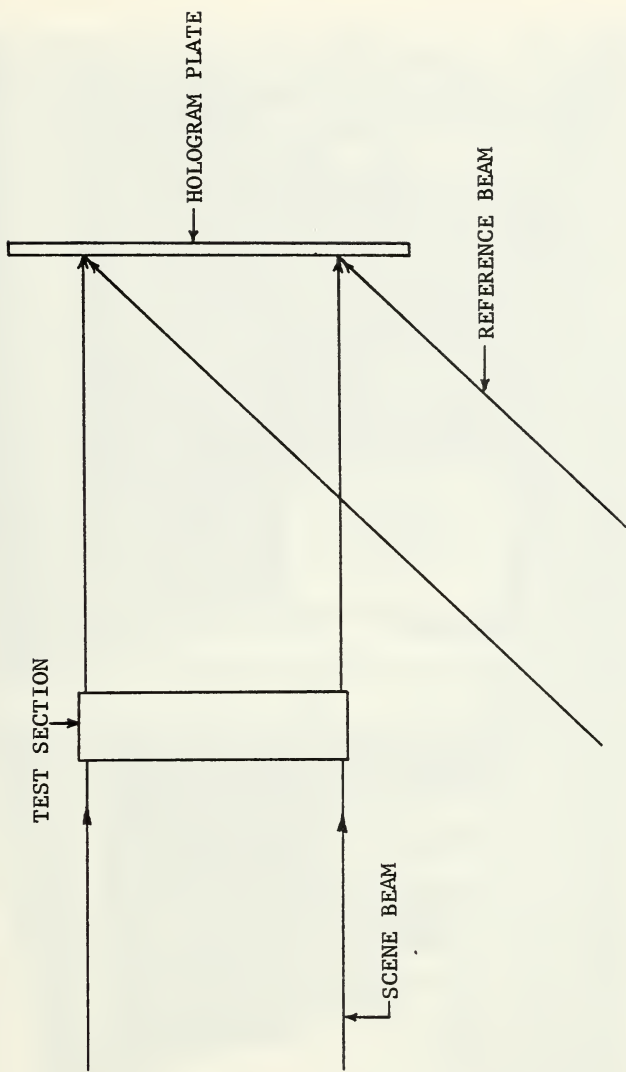
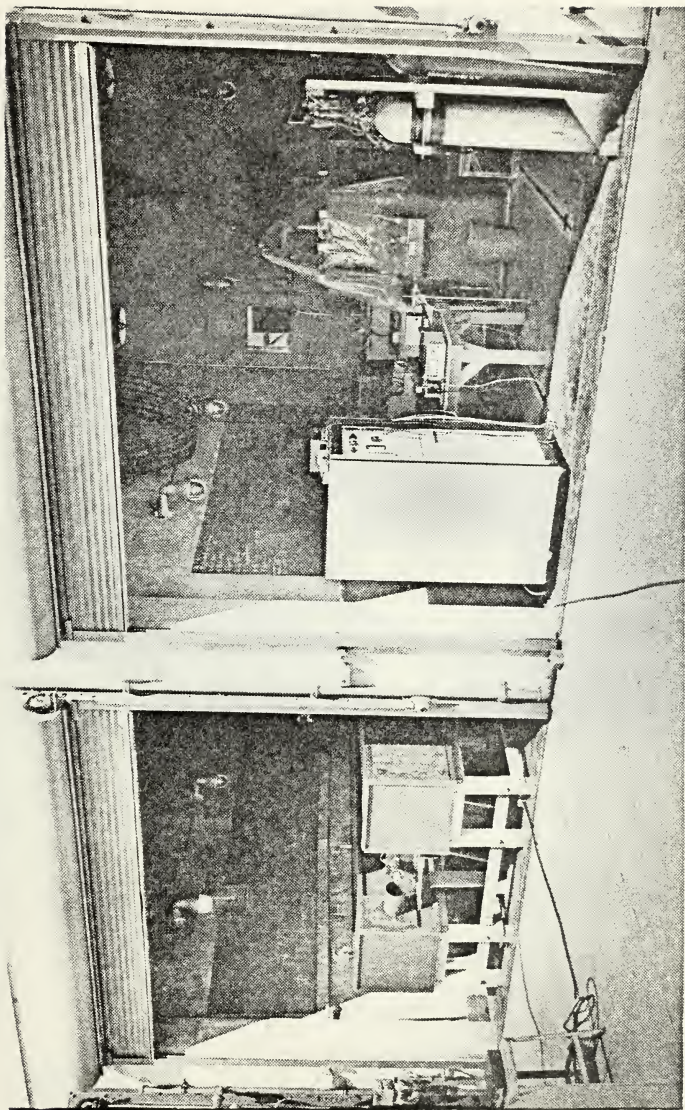


Figure 1. Direct Illumination Method of Obtaining a Hologram





Cannon and Optics Cell

Laser Installation

Figure 2



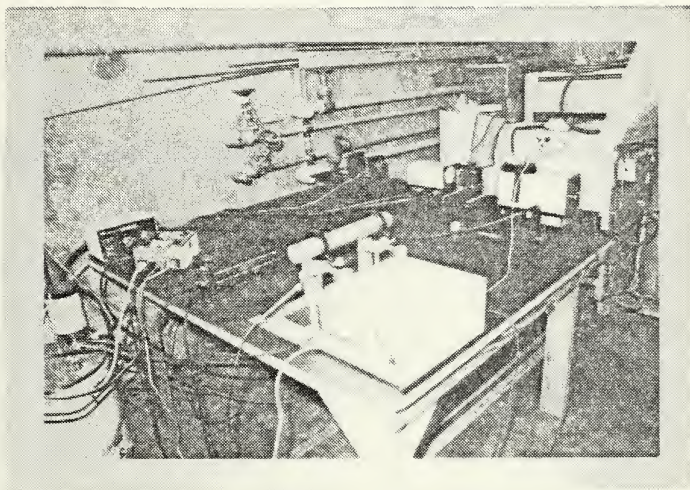


Figure 3. Laser Setup



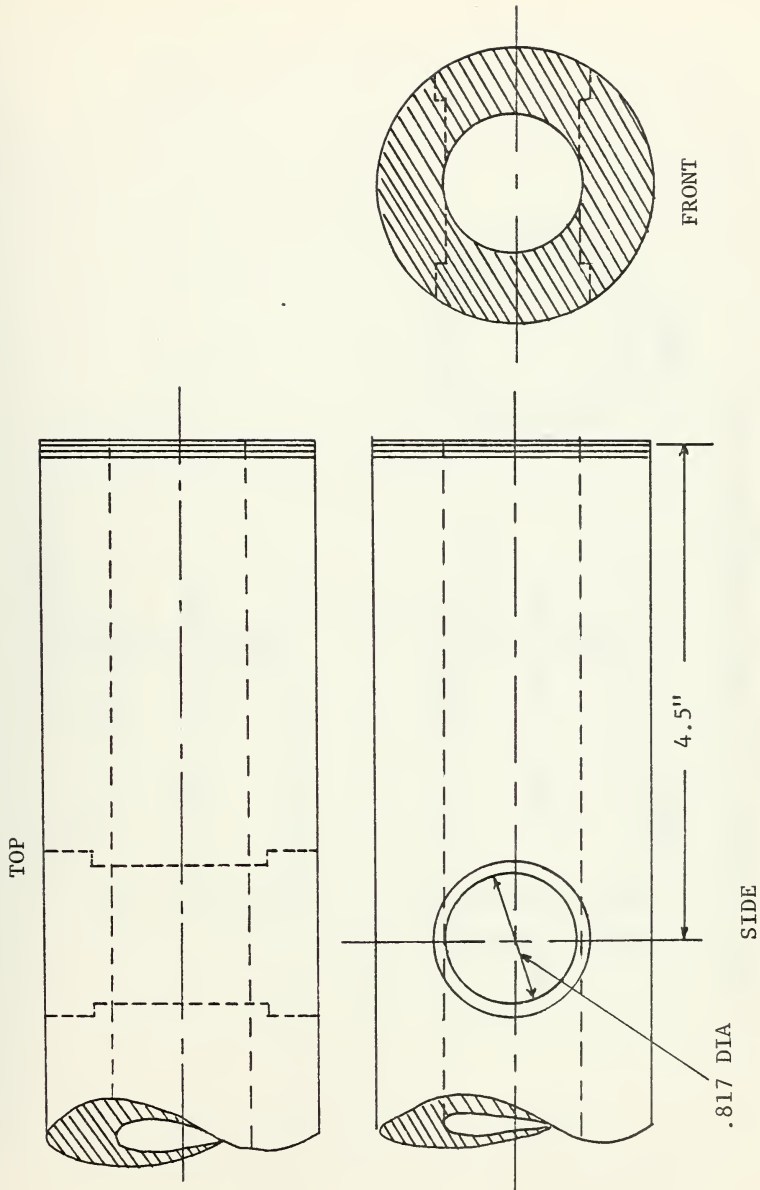
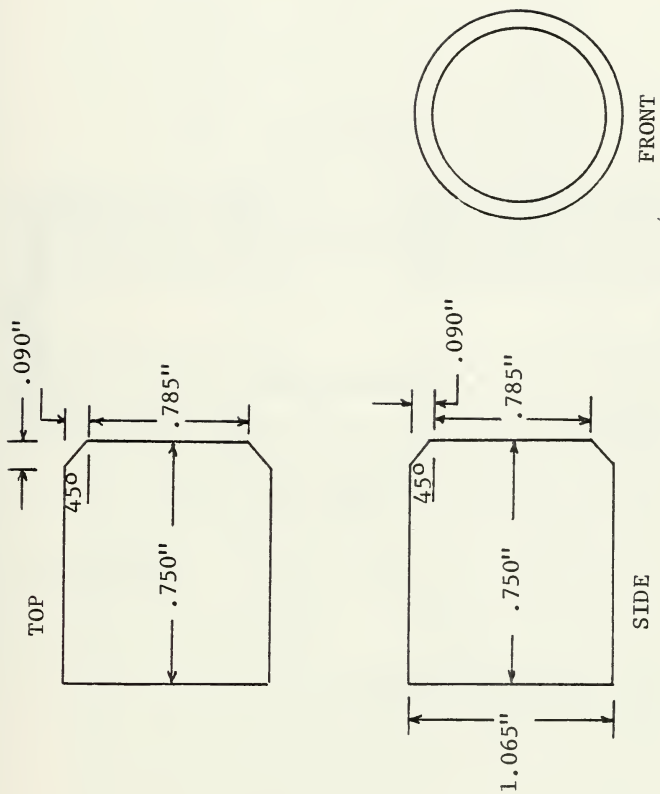


Figure 4. Barrel Design







NOTE: Windows to be seated with #118 O-ring

Figure 5. Plexiglass Windows



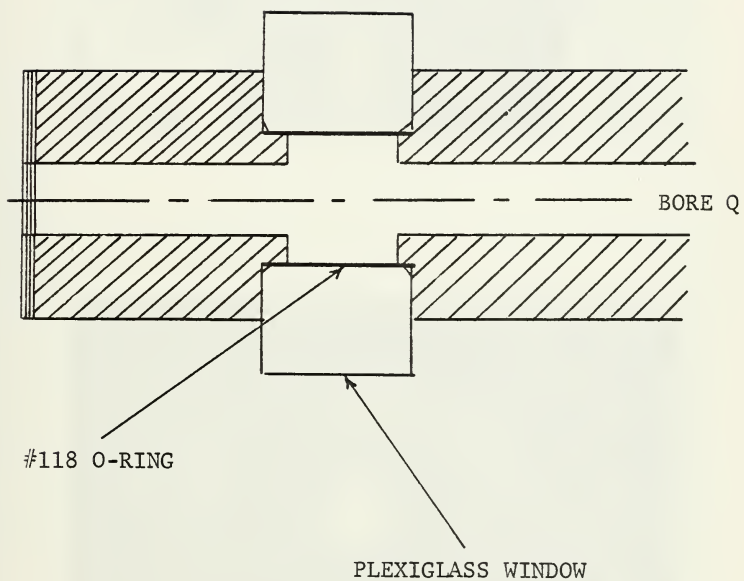


Figure 6.  
Top Cutaway View of Barrel with  
Plexiglass Window Installation



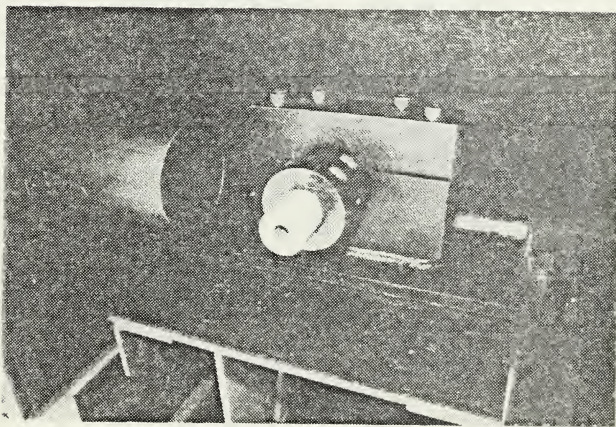


Figure 7. Barrel with Windows and with Collar



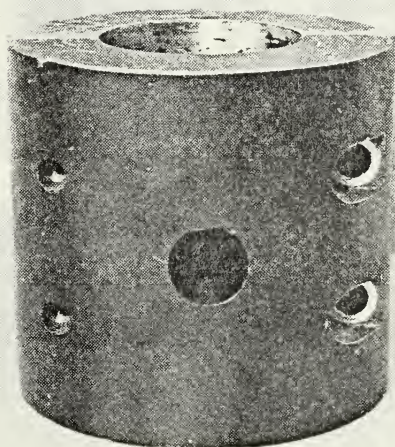
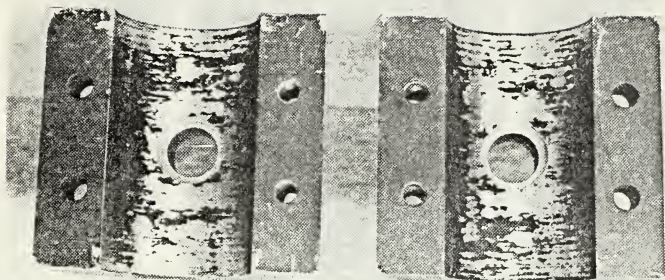


Figure 8. Collar Device





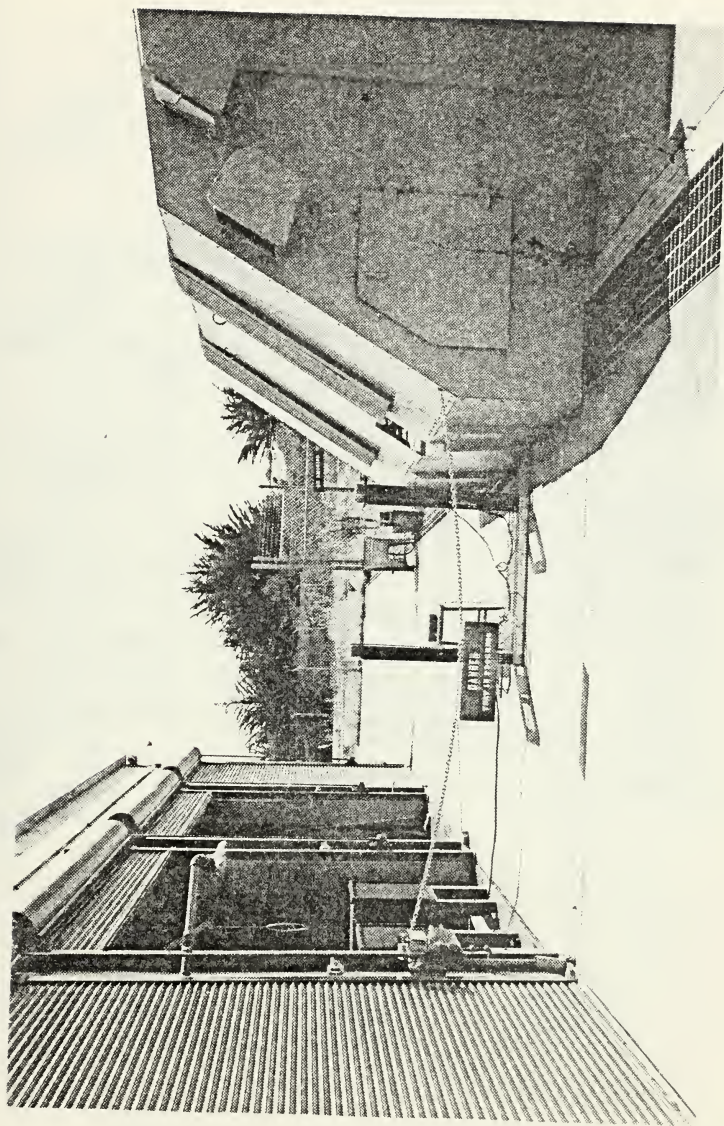


Figure 9. Projectile Path and Turret with Velocity Screen in Place



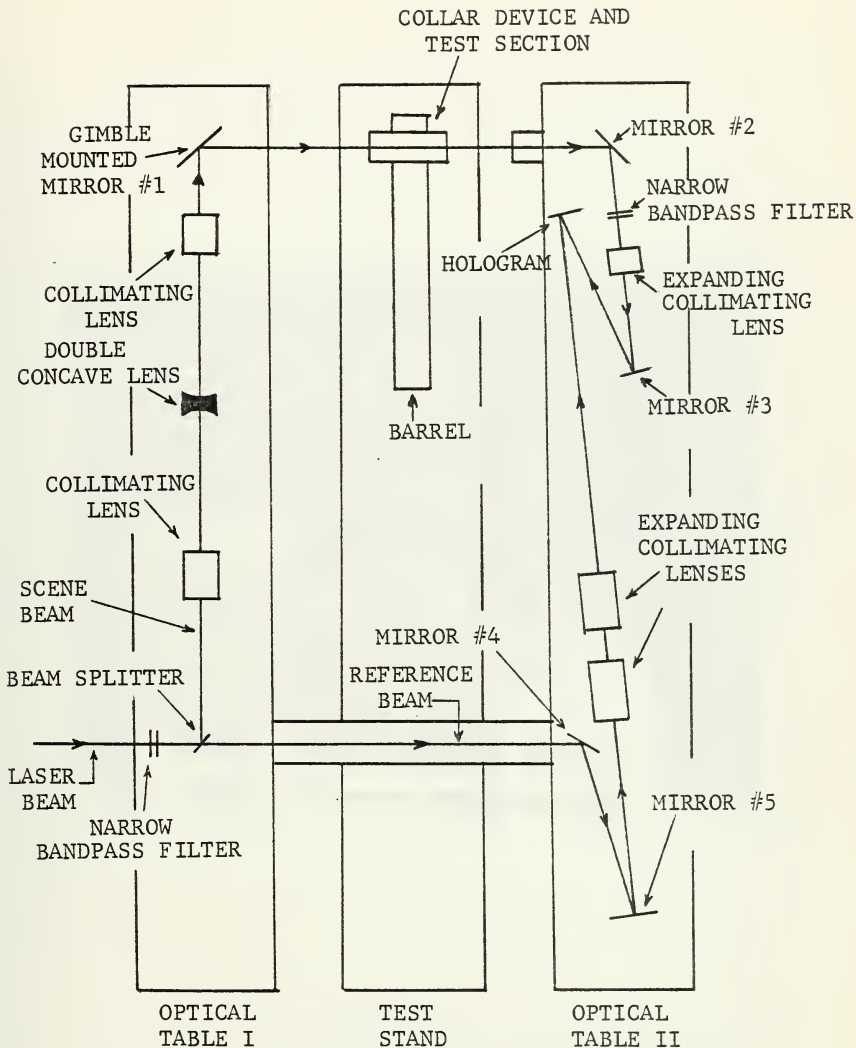


Figure 10. Optical Arrangement



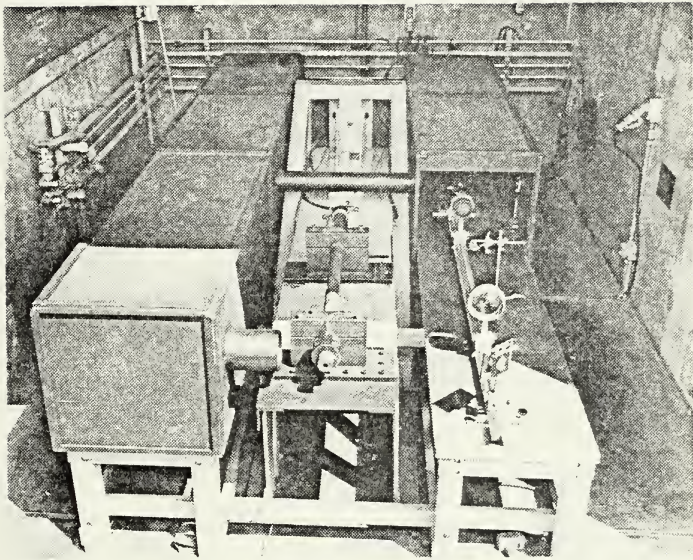


Figure 11. 20mm Cannon with Optical Platform



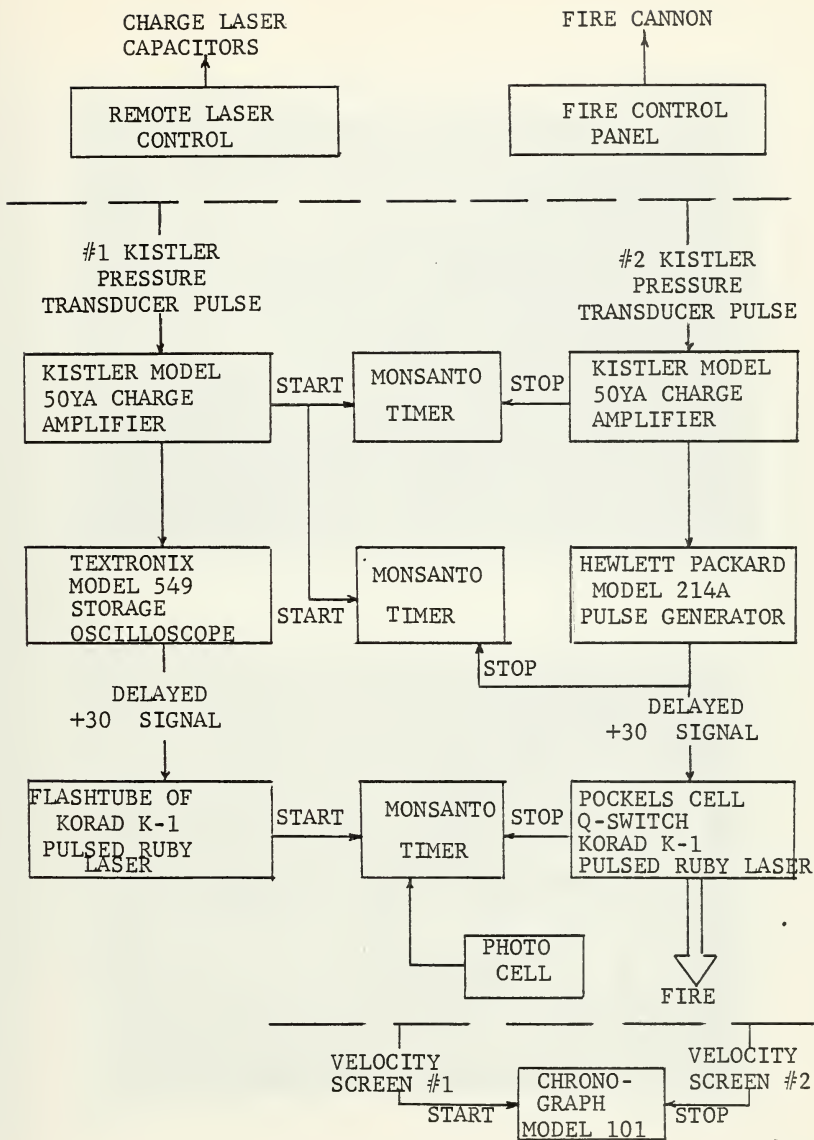


Figure 12. Firing Sequence







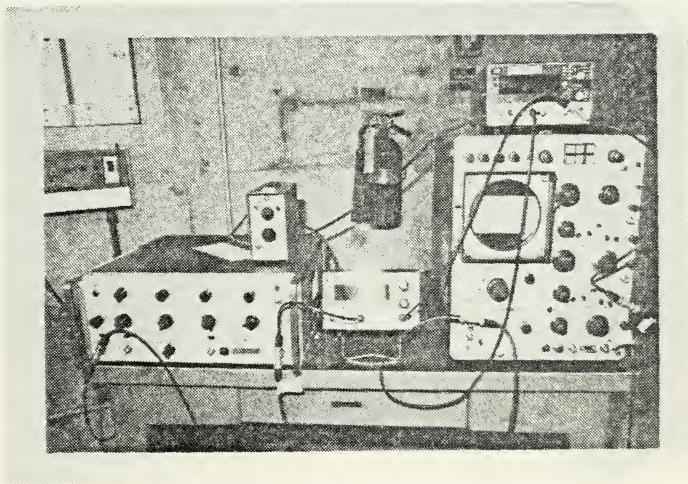
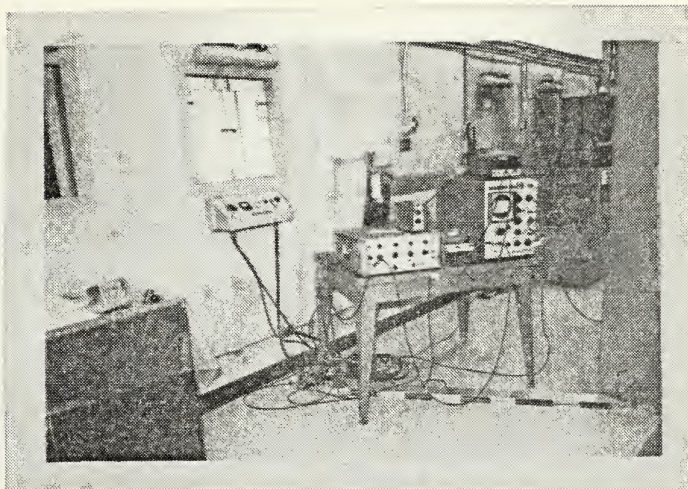


Figure 13. Control Room and Monitoring Equipment



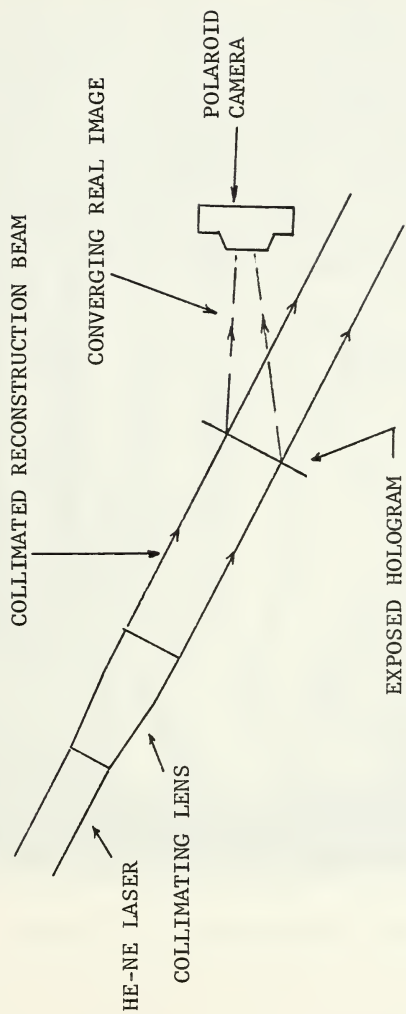


Figure 14. Reconstruction



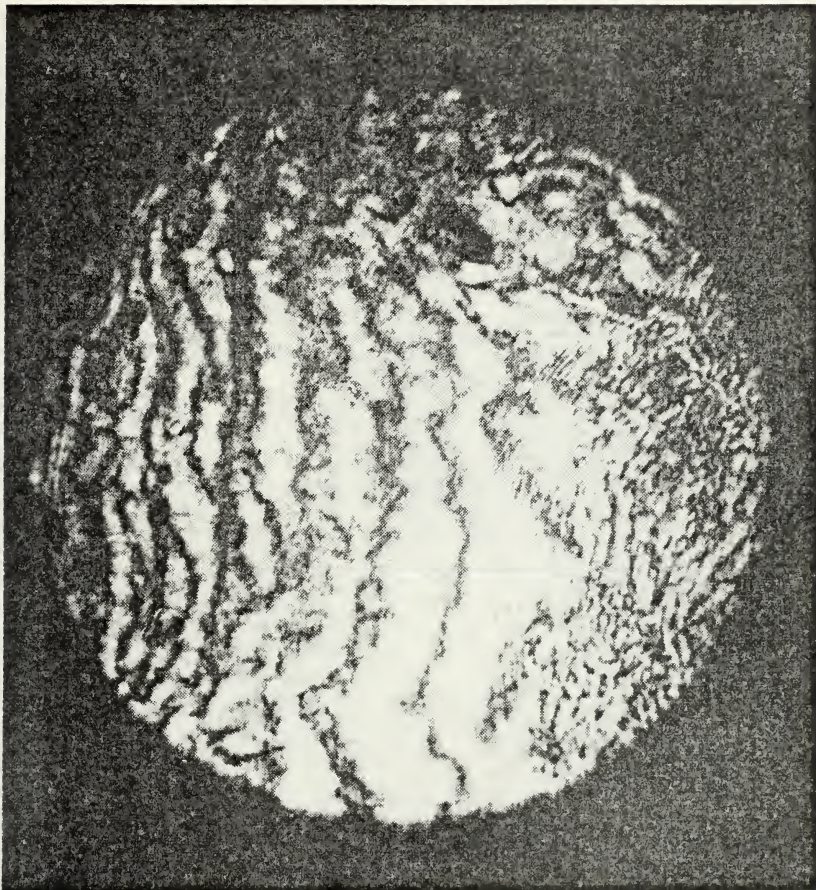


Figure 15. Compression Waves





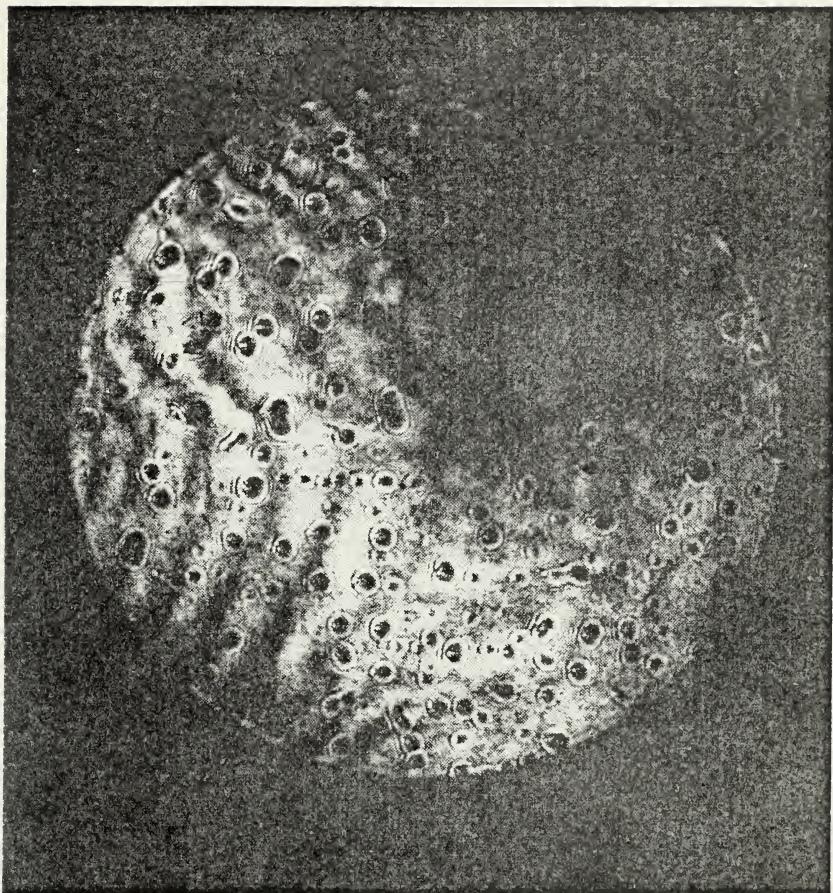


Figure 16. Compression Waves





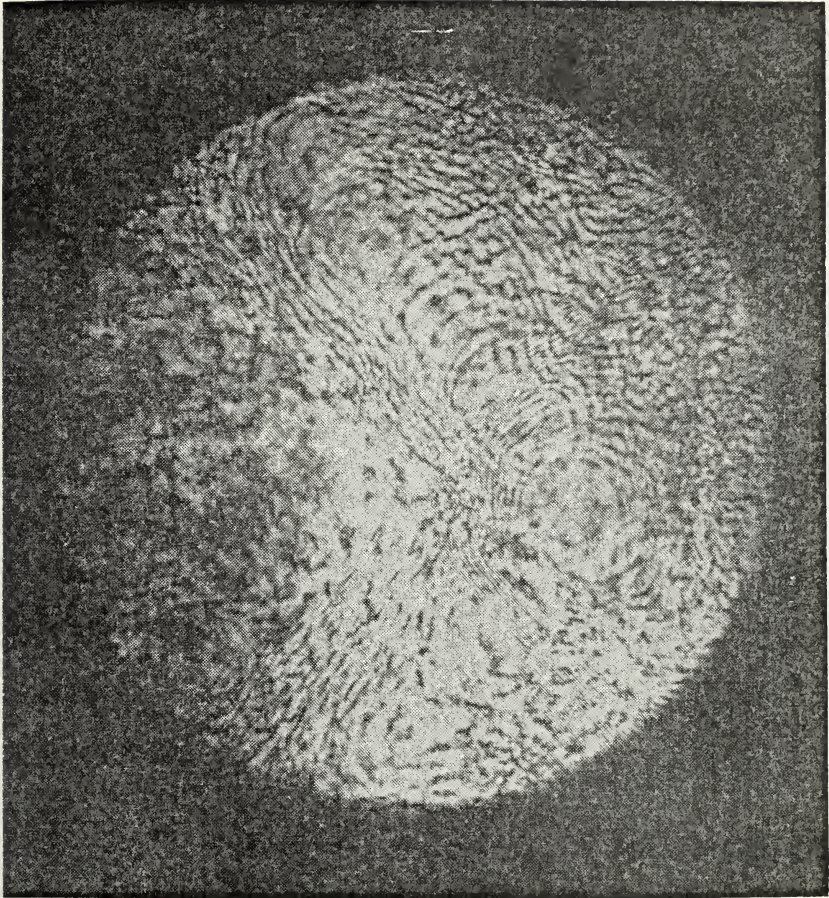


Figure 17. Bow Wave







Figure 18. Hologram Showing Carbon Deposits



### GUN BARREL PROJECT

Dimensions: 6 Regions, 6 Zones

<u>Regions</u>	<u>Zones</u>	<u>Length (cm)</u>	<u>Area (cmsq)</u>	<u>Volume (cc)</u>
1	1	1.47	2.95	4.35
2	1	1.47	2.95	4.35
3	1	1.47	2.95	4.35
4	1	1.47	2.95	4.35
5	1	1.47	2.95	4.35
6	1	5.40	2.95	15.93

### INITIAL CONDITIONS

Powder Conditions: Grams Powder = 38.23  
 TBURND = 1.00 Millisec

Materials:

<u>Region</u>	<u>NEQST</u>	<u>Pressure (psi)</u>	<u>Temp. (Deg. K)</u>	<u>Molec. Wt. (gm/mole)</u>
1	2	14.7	300.0	125.00
2	2	14.7	300.0	125.00
3	2	14.7	300.0	125.00
4	2	14.7	300.0	125.00
5	2	14.7	300.0	125.00
6	3	3.0	300.0	55.85

Print out every 0.20 millisec up to 10.00 millisec

Print out every 0.050 millisec up to break

Print out every 0.200 millisec up to launch

Mass of Projectile = 90.0 gm

Break Valve Strength = 690.0 Bars

Number of Pressure Points: 1

Location of Pressure Points: 14.0 cm

Figure 19. Computer Output Format



GUN BARREL PROJECT

Cycle 290	T(Millisecond)	1.88443E00	
	DT(Millisecond)	2.18257E-02	
j	X(CM)	VELOCITY (CM/MS)	PRESSURE (BARS)
1	0.0	0.0	1.01381E 03
2	1.46490E 02	1.01004E 02	8.52849E 02
3	1.47602E 02	1.03653E 02	7.78181E 02
4	1.48734E 02	1.06449E 02	8.85098E 02
5	1.49668E 02	1.07232E 02	1.05442E 03
6	1.50551E 02	1.06399E 02	3.98267E 02

Figure 20. Computer Output Format





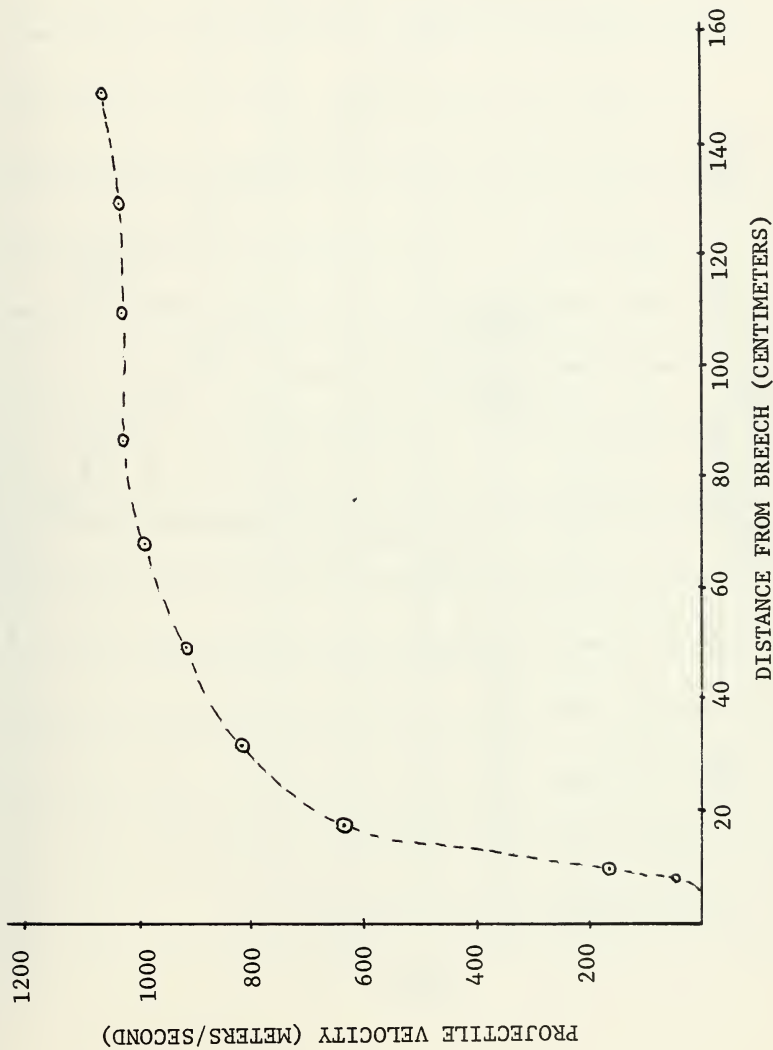


Figure 21. Projectile Velocity vs. Position



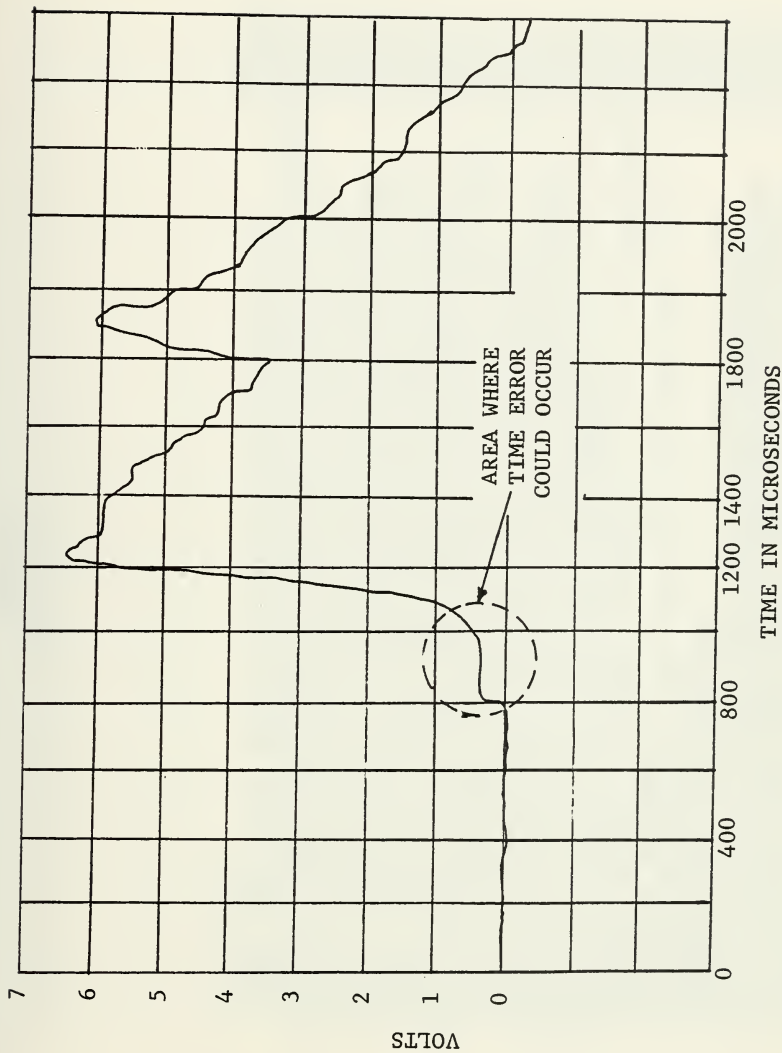


Figure 22. Pressure Trace Output from Pressure Transducer  
Locate 2.5 inches Aft of Observation Port







GUNNO037  
 GUNNO038  
 GUNNO039  
 GUNNO040  
 GUNNO041  
 GUNNO042  
 GUNNO043  
 GUNNO044  
 GUNNO045  
 GUNNO046  
 GUNNO047  
 GUNNO048  
 GUNNO049  
 GUNNO050  
 GUNNO051  
 GUNNO052  
 GUNNO053  
 GUNNO054  
 GUNNO055  
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 GUNNO060  
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 GUNNO066  
 GUNNO067  
 GUNNO068  
 GUNNO069  
 GUNNO070  
 GUNNO071  
 GUNNO072  
 GUNNO073  
 GUNNO074  
 GUNNO075  
 GUNNO076  
 GUNNO077  
 GUNNO078  
 GUNNO079  
 GUNNO080  
 GUNNO081  
 GUNNO082  
 GUNNO083  
 GUNNO086

```

T=0.0
ICATA=0
NI=0
123 M=6
DATA NREAD,NPRINT/5,6/
NEVTR=1
1 CALL ZEQAB
CALL ZEROA(500,XP1,XP2,PP1,VP2,XP3)
CALL ZEROA(500,PP3,PP1,PP1,PP1)
CALL ZEROA(10,ISTOPX,ISTOPX,ISTOPX,ISTOPX)
INTERJ(31)=M
CPMAX=0.0
PYMAX=0.0
ANEMAX=0.0
NTIIMPT=0
IF=0
NFUNCH=1
IPUNCHX=0
LN=0
IPV1=1
IPV2=2
C INITIAL CONDITIONS FOR PROGRAM, BEGIN INPUT FOR RUN,NEW OR ITE
IF(NPVTR.EQ.1)GO TO 41
NEVTR=1
C INPUT FOR ITERATION FROM STORAGE
CALL STORE(ISTORM,STORM)
EMLEAD=STORM(97)
HYDRD1=STORM(98)
HYDRD2=STORM(99)
NEGOST(30)=ISTORM(100)
IF(IDATA)8,8,608
41 CONTINUE
C INPUT FOR NEW RUN, STORAGE OF INPUT
READ(NREAD,604)IDATA,IPRNTZ,ITRNSF,IPUNCH,DTSQ(199)
604 FCFMAT(415,F10.0)
IF(ITRNSF.EQ.0) GO TO 619
M=6
INTERJ(31)=M
IF(IDATA)606,606,620
619 READ(NREAD,READ1)
608 ICATA=0
GO TO 610
606 CALL READ
READ(NREAD,20) IPOX, NPOX, (XPO(M), M=1, NPOX)
READ(NREAD,49) XPV2, PVERK, PVWANT
READ(NREAD,61R,EMPIST, FRAC, EMLEAD
FCFORMAT(E10.4,3F10.0)
6 READ (NREAD,49) (AMOL(I),I=1,IMAX)
    
```





GUNNO085  
 GUNNO084  
 GUNNO087  
 GUNNO088  
 GUNNO089  
 GUNNO090  
 GUNNO091  
 GUNNO092  
 GUNNO093  
 GUNNO094  
 GUNNO095  
 GUNNO096  
 GUNNO097  
 GUNNO098  
 GUNNO099  
 GUNNO100  
 GUNNO101  
 GUNNO102  
 GUNNO103  
 GUNNO104  
 GUNNO105  
 GUNNO106  
 GUNNO107  
 GUNNO108  
 GUNNO109  
 GUNNO110  
 GUNNO111  
 GUNNO112  
 GUNNO113  
 GUNNO114  
 GUNNO115  
 GUNNO116  
 GUNNO117  
 GUNNO118  
 GUNNO119  
 GUNNO120  
 GUNNO121  
 GUNNO122  
 GUNNO123  
 GUNNO124  
 GUNNO125  
 GUNNO126  
 GUNNO127  
 GUNNO128  
 GUNNO129  
 GUNNO130  
 GUNNO131  
 GUNNO132

```

READ (NREAD,49) (TO(I),I=1,IMAX)
READ (NREAD,49) (PO(I),I=1,IMAX)
45 FORMAT(7F10.0)
610 CONTINUE
CALL STORM (ISTORM, STORM)
STORM(97)=EMLEAD
STORM(98)=HYDRD1
STORM(99)=HYDRD2
ISTORM(100)=IPOX
INITIAL CONDITIONS AND CONSTANTS FOR RUN
C 8 NP1=NZONES(1)+NZONES(2)+NZONES(3)+1
XSTT=FRAC*OUTBDY(5)
NEGST(30)=IPOX
CALL CALCUL (EMLEAD)
IF (N1.NE.0) GO TO 603
CALL PRINT (EMLEAD,FRAC,XPV1,XPV2,PVWANT,NPCX,IPCX,XPG)
IF (LPRINT.EQ.0) GO TO 603
REAL (NREAD,1) ILASTK
IF (ILASTK) 123,12,1
603 CALL SETUP
DO 706 IMP=1, JLAST
PMDMIN(IMP)=PPLUSQ(IMP)
PMDMAX(IMP)=PPLUSQ(IMP)
C 706 MAIN LOOP OF PROGRAM - DYN,REQ, LFTOVER, AND OUTPUT
2 CALL DYNREQ
CALL LFTOVR (IPNCHX)
DO 710 IMP=1, JLAST
IF (PPLUSQ(IMP).GT.PMDMIN(IMP)) GO TO 705
PMDMIN(IMP)=PPLUSQ(IMP)
TMDMIN(IMP)=T
C 705 IF (PPLUSQ(IMP).LT.PMDMAX(IMP)) GO TO 710
PMDMAX(IMP)=PPLUSQ(IMP)
TMDMAX(IMP)=T
710 CONTINUE
IF (IPUNCH.EQ.0 .OR. PROJ.NE.300) GO TO 627
PRSTAB(NPUNCH)=T-DTSQ(200)
NP1=NPUNCH+1
JPLFAF=INTERJ(6)
J=JPLHAF
JMHAF=JPLHAF-1
DUDI=26./18.*PPLUSQ(JMHAF)-1./9.*PPLUSQ(JMHAF-1)
C 707 PRSTAB(NP1)=DUDI
IF (T.GT.(DTSQ(200)+DTSQ(199))) GO TO 647
PRSTAB(NP1)=PRSTAB(NP1)*(T-DTSQ(200))/DTSQ(199)
C 647 NPUNCH=NPUNCH+2
IF (51-NPUNCH) 625,625,627
C 625 PUNCH 641 PRSTAB
C 641 FORMAT(3(F12.8,E12.8))
    
```



```

NPUNCH=1
627 CONTINUE
630 M=6
72
C CONTINUE OF MAXIMUM PRESSURES
  INER51 = INTERJ(6) -1
  CPMAX = AMAX1(CPMAX, PPLUSQ(NPTN-1))
  PPMAX = AMAX1(PPMAX, PPLUSQ(INER51))
  AMPMAX = AMAX1(AMPMAX, PPLUSQ(INER51))
C DETERMINATION IF MODEL HAS BEEN LAUNCHED
  IF(XSTOP-X(JLAST, NPLUS1)) 9, 3, 3
C ROUTINE STORAGE OF POINTS TO BE PLOTTED
  3 IF(IPOX.EQ.5) GO TO 2
  KN = NCYCLE/6
  CN = KN
  SN = NCYCLE
  TN = SN/6
  IF(TN-UN) 4, 4, 2 GO TO 7
  4 IF(LN.GT.498) GO TO 7
  LN = LN + 1
  IF(IPOX.EQ.6) GO TO 75
  XP3(LN) = T
  PP3(LN) = PPLUSQ(NPTN)
  XP4(LN) = X(NPTN-1, N)
  PP4(LN) = PPLUSQ(NPTN-1)
  IF(IPOX.EQ.1) GO TO 51
  DQ GO TO INPOX=1, NPOX
  IF(ISTOPX(INPOX).GE.1) GO TO 60
  NTIMPT=LN
  DC 58 INPTN=2, JLAST1
  IF(XPO(INPOX).LT.X1(INPTN)) GO TO 59
  58 CONTINUE
  DUMVAR(LN, INPOX) = PPLUSQ(INER51)
  NPTPL(INPOX) = LN
  GO TO 60
  59 DUMVAR(LN, INPOX) = PPLUSQ(INPTN)
  1/(X1(INPTN-1)-X1(INPTN))*XPO(INPOX)-X1(INPTN-1)
  NPTPL(INPOX) = LN
  IF(LN.EC.1099) GO TO 55
  GO TO 60
  55 ISTOPX(INPOX) = 2
  NPTPL(INPOX) = LN
  CONTINUE
  60 IF(IPOX.NE.6) GO TO 78
  75 DUMVAR(LN, 1) = PPLUSQ(INER51)
  78 IPOX(LN) = 1
  IF(IPOX.EQ.6) GO TO 2

```

GUNNO133  
 GUNNO134  
 GUNNO135  
 GUNNO136  
 GUNNO137  
 GUNNO138  
 GUNNO139  
 GUNNO140  
 GUNNO141  
 GUNNO142  
 GUNNO143  
 GUNNO144  
 GUNNO145  
 GUNNO146  
 GUNNO147  
 GUNNO148  
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 GUNNO164  
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 GUNNO170  
 GUNNO171  
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 GUNNO173  
 GUNNO174  
 GUNNO175  
 GUNNO176  
 GUNNO177  
 GUNNO178  
 GUNNO179  
 GUNNO180



```

51 IF(IPOX.EQ.2) GO TO 52
C PROGRAM TO FIND MAX IN REGION TO GO HERE
52 CONTINUE
C
C STORAGE OF MODEL PLOTS AFTER BREAK VALVE
5 IF(JPROJ-300) 13,5,13
7 IF(IP.GT.498) GO TO 2
IP=IP+1
IF(XSTOP.EQ.3000.) GO TO 76
10 XP(IP)=X(JLAST,N)
XP2(IP)=X(JLAST,N)
PP1(IP)=PPPLUSQ(INER51)
VP2(IP)=U(JLAST, NMNHAF)
GO TO 2
C
C POINT OF RETURN TO MAIN LOOP OF PROGRAM
C FINAL STORAGE OF POINTS TO BE PLOTTED, AND WRITING OF ALL PLOT TAPES
9 IF (IPOX.EQ.5) GO TO 25
IF (IPOX.EQ.6) GO TO 76
IP=IP+1
XP(IP)=X(JLAST,N)
XP2(IP)=X(JLAST,N)
PP1(IP)=PPPLUSQ(INER51)
VP2(IP)=U(JLAST, NMNHAF)
GO TO 36
35 NPOX=1
36 DO 70 IPLTXT=1,NPOX
NPTIX=NPTPL(IPLTXT)
IF(NPTIX.LT.10) GO TO 70
NPTIT=NPTPL(IPLTXT)
DO 90 IIXP=1,NPTIT
IPL(IIXP)=IPOX(IIXP)
PPL(IIXP)=DUMVAR(IIXP, IPLTXT)
IF(JPROJ.NE.300) GO TO 1
70 CONTINUE
GO TO 25
76 DO 93 IXP=1, LN
93 PPL(IIXP)=DUMVAR (IIXP,1)
TERMINATION OF RUN; RETURN FOR NEW INPUT
C
25 READ(INREAD,1) ILASTK
IF((IPUNCH.EQ.0).OR.(NPUNCH.EQ.1)) GO TO 629
NPUNCH=NPUNCH-1
PUNCH 641, (PRSTAB(IPXX), IPXX=1,NPUNCH)
625 CONTINUE
WRITE(6,45) CPMAX, PTMAX, AMPMAX
704 FORMAT(13,2X,E12.6,2X,E12.6,2X,E12.6,2X,E12.6)
45 IF(ILASTK) 15, 12, 1

```

GUNNO181  
 GUNNO182  
 GUNNO183  
 GUNNO184  
 GUNNO185  
 GUNNO186  
 GUNNO187  
 GUNNO188  
 GUNNO189  
 GUNNO190  
 GUNNO191  
 GUNNO192  
 GUNNO193  
 GUNNO194  
 GUNNO195  
 GUNNO196  
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 GUNNO198  
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 GUNNO211  
 GUNNO212  
 GUNNO213  
 GUNNO214  
 GUNNO215  
 GUNNO216  
 GUNNO217  
 GUNNO218  
 GUNNO219  
 GUNNO220  
 GUNNO221  
 GUNNO222  
 GUNNO223  
 GUNNO224  
 GUNNO225  
 GUNNO226  
 GUNNO227  
 GUNNO228



```

15 WRITE(6,44)(NI,((AVEL(I),ALOAD(I),AGAS(I)),I=1,NI))
16 GO TO 123
17 STOP
18 FORMAT (2I2,7F10.0)
19 FORMAT (I3/13F10.0)
44 END
11 END
SUBROUTINE READ
  REAL*8 DIMENSIONS, INITIAL CONDITIONS, AND PGWDR PARAMETERS
  COMMON AREA1, DLAMDA, DT SQ, AREA2, CMA, XRS, CQ, CSMAX, CP, CV, DLAMAX,
  1 DPMIN, DQ1, DQ2, DQ3, EZERO, EINF, SUM, EINT, EKIN, H, ETOI, ETEINTH,
  3EWRONG, EL, FORCE, GAMMA, HCFM, HALFRD1, HYDRD2, HYDRD3, SHPR,
  4OUTBODY, OUTDT1, OUTDT2, PCON1, PCON2, PPLUSQ, P, P1, Q, ROZ, SIGSQ, T, NEXT,
  5SIGMAX, SIGMIN, SKIN, TMAX2, TVD1, TVD2, TBAR, TVRE, THETA, TMAX1,
  6TPRINT, TVNEX, TMIN, TSO, TVFEQ, UZERO, U, USQ, XMAX, XMIN, XTOP,
  7VZERO, V, VOL, XDM, VISCS, X, XINDEX, XMIN, XMAX, XPROJ, X2, XMIN, XMAX, J,
  8COMMON IMAX, INU, IZ, JLAST, JMIN, JMAX, K, L, LACHSQ, NDATEI, NDAT E2,
  1 JPHAF, JMHAF, JNV, NCHEKE, NEGST, NZONES, NCYCLE, N, NMNHAF, NPLUS1,
  2NDATE3, NUMBER, NPL3HF, NP, IQUIT, JSTOP, KEMP, LST, PC, CV(30), CV(30),
  3NPHAF, NN, NPL3HF, NN, NPL3HF, NN, NPL3HF, NN, NPL3HF, NN, NPL3HF, NN,
  DIMENSION AREAMDA(200,2), CQSQX(30), CMAXR(30), CSQ(200), CP(30), CV(30),
  1DTMIN(30), DEAMDA(200), DTSQ(200), DELX(30), DQ1(200), DQ2(200), DS(200),
  2ZER0(30), EI(200,2), EINT(30), EKIN(30), FORCE(30), GAMMA(30),
  3HALFEM(30), HALFRD(30), HYDRAD(200), INFERJ(31), MACHSQ(200), NEGST(30),
  4NZONE(30), OUTBODY(30), PPLUSQ(200), PL(200,2), ROZERO(30),
  5XKIN(200), SIGSQ(200), TMIN, TVD1, TVD2, TVRE, THETA(200), UZERO(30),
  6U(201,2), USQ(201), VZERO(30), V(200,2), VISCS(200), X(201,2), X1(200),
  7ZMACHSQ(200), ZPU(30), ZT(30), ZT(30), ZT(30), DUMVAR(500,5)
  1 FORMAT(20I3)
  2 FCRMAT(F10.0, 15)
  3 READ(NREAD,1) IMAX, NDATE1, NDATE2, NDATE3, NUMBER, NCHEKE, INU, JPRCJ
  READ(NREAD,1) (NEOST(I), I=1,IMAX)
  READ(NREAD,1) (NZONES(I), I=1,IMAX)
  READ(NREAD,1) (OUTBODY(I), I=1,IMAX)
  READ(NREAD,3) (GAMMA(I), I=1,IMAX)
  READ(NREAD,3) (CQSQX(I), I=1,IMAX)
  READ(NREAD,3) AREA1, AREA2, AREA3, PCON1, PCON2, SHPR, EMPROJ
  READ(NREAD,3) OUTDT1, IMAX1, OUTDT2, TMAX2, XSTCP
  8 IF(INU) 9, 901, 9
  9 READ(NREAD,3) (UZERO(I), I=1,IMAX)
  901 DO 902 I=1,IMAX
  902 UZERO(I)=0.
  904 READ(NREAD,100) PCON3, SLOPE, RADIUS

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READ(NKREAD,5),ICALPGM,TBURND,GMS PDR,GASPRS,IHEL
READ(NKREAD,1,23) HYDR01,HYDRD2
FORMAT(2E15.5)
WRITE(6,123)HYDRD1,HYDRD2
5 WFORMAT(4F10.0,I4)
903 RETURN
END
SUBROUTINE PRINTO(EMLEAD,FRAC,XPV1,XPV2,PVWANT,NPOX,IPOX,XPO)
PRINT DIMENSIONS AND POWDER CONDITIONS
COMMON PCON3,SLOPE,RADIUS,AREA,CSQX4,CMAXR,CSQ,CSQMAX,CP,CV,DLAMAX,
1,DTMIN,DUDT,DLAMDA,DTSQ,TLAST,DLAST,DJLAST,DMU,DPDE,DELX,ENTH,
3EWRONG,CQ1,DQ2,DS,EZER,ESUM,EKIN,EKIN,ETOT,ENTH,
4OUTBODY,EL,FORCE,GAMMA,HALFM,HALFKO,HYDRD2,HYDRD3,HYDRAD,
5SIGMAX,SKINDT,SKIN1,MAX2,TVD1,TVD2,TMAX,TS,GSQ,TNEXT,
6TPRINT,TVNEAT,MINCO,TVFREQ,UZERO,U,USQ,TBAR,TVKEL,XTWALL,
7VZEROS,VOLUME,VISCOSEX,XI,SEID,XMIN,XPMAX,ZMASS,ZEMPRD,XSTOP,
COMMON IMAX,INU,IN,INTERJ,INDEX,ILIMN1,JPROJ,JPJRCJZ,MIN,IMAXFJ,
1JPLHAF,JMNHAF,JUST,JLAST,JLAST1,JMIN1,K,L,MACHSQ,NDATE1,NDATE2,
3NPLHAF,NN,NPL3HF,NP,2,CQSQX4(30),CMAXR(30),EMPIS1,PO,HTO,AMOL,DUMVAR
DIMENS(3),DLAMDA(200),DTSQ(200),DELX(30),DGL(200),DC2(200),DS(200),GMMVA(30),
1E(200),2),EIN(30),EKN(30),FERJ(31),MACHSQ(200),NEQST(30)
3HALFK(200),4OUTBODY(30),HYDRAD(200),INFERJ(31),MA(200),ROZRO(30),
5KZONES(30),6OUTBODY(30),PPLUSQ(200),TVKEL(30),TVKEL(30),UZERO(30),
7ZINI(200),USQ(200),IMINSQ(2),TVKEL(30),TVKEL(30),UZERO(30),
6ZMASS(200),PO(30),TO(30),AMOL(30),DUMVAR(500),5)
DIMENSION XLGTH(30),ZOMASS(30),XPO(10),REGVCL(30)
WRITE(6,65)
FORMAT(1H1)
FGLGTH(1)=OUTBODY(1)
REGVCL(1)=AREAL*XLGTH(1)
IF(IMAX.EQ.1) GO TO 210
DO 200 KQX=2,IMAX
XLGTH(KQX)=OUTBODY(KQX)-OUTBODY(KQX-1)
KQX=IMAX-1
201 KQX=2,KQX=2,KQX
DU REGVCL(KQX)=AREA*XLGTH(KQX)
210 REGVCL(IMAX)=AREA*XLGTH(IMAX)
REGVCL=AN(SLOPE)
ANGLE=ANGLE#(360./6.2832)
WRITE(6,100) NUMBER,NDATE1,NDATE2,NDATE2
WRITE(6,102) IMAX,JPROJ
I=1
    
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WRITE (6,103) I,NZONES(I),XLGTH(I),AREAL,REGVOL(I)
IF (IMAX.EQ.1) GO TO 211
KCX=IMAX-1
WRITE (6,103) (I,NZONES(I),XLGTH(I),AREA2,REGVOL(I),I=2,KCX)
WRITE (6,103) IMAX,NZONES(IMAX),XLGTH(IMAX),AREA3,REGVOL(IMAX)
WRITE (6,105) SLOPE,ANGLE
WRITE (6,111) CALPGM,TBURND,GMS PCR,GASPRS
WRITE (6,106)
WRITE (6,108) (I,NEQST(I),PO(I),TO(I),T0(I),AMOL(I),CQSQX4(I),I=1,IMAX)
WRITE (6,109)
WRITE (6,110) (I,GAMMA(I),EZERO(I),ROZERO(I),VZERO(I),I=1,IMAX)
WRITE (6,124) R
WRITE (6,114) XPV1,XPV2,PVWANT
WRITE (6,115) OUTDT1,TMAX1,OUTDT2,TMAX2
EMLEAX=EMLEAD*453.59
EMPISX=EMPISL*453.59
XXMAS=REGVOL(IMAX)*ROZERO(IMAX)
SHPRX=SHPR#14.5D4
WRITE (6,112) EMLEAD,EMLEAX,EMPIST,EMPISX,XXMAS
WRITE (6,113) SHPR,SHPRX
KQX=IPOX+1
GO TO (10,11,12,12,13,14),KQX
10 WRITE (6,119) IPOX
GC TO 15
11 WRITE (6,120) IPOX
GC TO 15
12 WRITE (6,123) IPOX
GC TO 15
13 WRITE (6,121) IPOX
GC TO 15
14 WRITE (6,122) IPOX
15 WRITE (6,116) NPOX
WRITE (6,117) (XPO(I),I=1,NPOX)
WRITE (6,118) FRAC
WRITE (6,65)
RETURN
100 FORMAT (2X,36HYPERVELOCITY MODEL LAUNCHER PROGRAM//2X,19HCOMPUTE,
101 IR, RUN NUMBER,15 TH DATE,12 IH/,12,1H/,12)
102 FORMAT (1H/34X,14HGUN DIMENSIONS,31X,12,10H REGIONS ,13,6H ZONE$GUNNO303
1//12X,6HREGION,5X,5HZONES,6X,6HLENGTH,9X,4HAREA,11X,6HVOLUME/35X,4
2H(CM) 9X,6H(CMSQ),11X,4H(CCC/1H)
103 FCORMAT (14X,12,9X,12,2X,F10.2,5X,F10.2,7X,F10.2)
104 FCORMAT (14X,12,9X,12,2X,F10.2,11X,3H---,12X,3H---)
105 FCORMAT (1H/19X,7HSLOPE =,F8.4,9X,5HANGLE =,F6.2,5H DEG)
106 FCORMAT (1H/5X,12HATERIALS --//7X,6HREGION,5X,5HNEQST,5X,8HPRESSUR$GUNNO309
15X,4HTEMP,9X,8HMOLEC WT,6X,6HCSQX4/30X,5F(P$),6X,7H(DEG K),7X,
29H(GM/MOLE)/1H)
108 FORMAT (9X,12,8X,12,5X,F9.2,6X,F7.2,6X,F9.4,6X,F5.1)
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109 FORMAT(1H /6X,6HREGION 4X,5HGAMMA,9X,6HENERGY,10X,7HDENSITY,9X,9HSGUNNO373
1P VOLUME/26X,13H(BARS-CC/CCO),7X,7H(GM/CC),5X,8H(CC/CCO)/1H )
GUNNO374
110 FORMAT(8X,12,5X, F,6,3,6X, E11,4,5X,E11,4,6X,E11,4)
GUNNO375
111 FORMAT(1H //32X, 18HINITIAL CONDITIONS/5X,20HPOWDER CONDITONS --//GUNNO376
114,8HCAL PCM =,F12,4,6X,8HBTBURN =,F12,4,6H MSEC/14X,8HGMSPOD =,F12,4,6H
GUNNO377
212,4,6X,8HGASPRS =,F12,4,5H PSI)
GUNNO378
112 FORMAT(1H //5X,10HEIGHTS --//9X,6HPHISTON/13X,23HMASS OF FIRST SECT/GUNNO379
11CN =,F13,4,4H LB,8X,1H=,F13,4,4H GM/13X,24HMASS OF SECOND SECT/GUNNO380
20N =,F12,4,4H LB,8X,1H=,F13,4,4H GM//9X,15HMODEL/13X,15HPASS OF 3R/GUNNO381
30CEL =,F12,4,4H (CM)
GUNNO382
113 FORMAT(1H //18X,22HBREAK VALVE STRENGTH =,F10,2,6H BARS,5X,1H=,F10,2,6H
GUNNO383
1,2,15H PSI)
GUNNO384
114 FCMAT(1H //5X,18HPHISTON VELOCITY --//10X,6HXPV1 =,F10,2,7H CM
GUNNO385
110X,6HXPV2 =,F10,2,7H CM //10X,18HDESIRED VELOCITY =,F10,2,7H FT/GUNNO386
2/SECC)
GUNNO387
115 FDMAT(2H //20X,15HPRINT OUT EVERY,F7,3,11H MSEC UP TO,F7,3,5H MSEC/GUNNO388
1EY,20X,15HPRINT OUT EVERY,F7,3,11H MSEC UP TO LAUNCH)
GUNNO389
2UI EVERY,F7,3,18H MSEC UP TO LAUNCH)
GUNNO390
116 FORMAT(1H //10X,26HNUMBER OF PRESSURE POINTS,14//10X,27HLOCATION O/GUNNO391
1F PRESSURE POINTS)
GUNNO392
117 FORMAT(20X,F9,2,3H CM) START FRACTION ,1PE11.4)
GUNNO393
118 FORMAT(1H //10X,20HPLOT --,10X,6HIPOX =,13,34H (ALL PLOTS, ALL PRES/GUNNO394
119 FORMAT(1H //5X,8HPLOTS --,10X,6HIPOX =,13,34H (ALL PLOTS, NO PRES/GUNNO395
1SSURE POINTS))
GUNNO396
120 FDMAT(1H //5X,8HPLOTS --,10X,6HIPOX =,13,32H (ALL PLOTS, NO PRES/GUNNO397
1S/SECC POINTS))
GUNNO398
121 FDMAT(1H //5X,8HPLOTS --,10X,6HIPOX =,13,12H (NO PLOTS))
GUNNO399
122 FORMAT(1H //5X,8HPLOTS --,10X,6HIPOX =,13,24H (ONLY PRESSURE POIN/GUNNO400
1S))
GUNNO401
123 FORMAT(1H //5X,8HPLOTS --,10X,6HIPOX =,13)
GUNNO402
124 FORMAT(1H //6X,3HR =,1PE11.4)
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5 SKIN(200),TSIGSQ(200),TMINSQ(2),TOVREL(30),THETA(200),UZERO(30),
6 U(20),U(20),USQ(20),V(200),VZERO(30),V(200),VISCOS(200),X(20),X(20),X(200),
7 ZMSS(200),PUL(30),PUL(30),A(30),A(30),A(30),A(30),A(30),A(30),A(30),A(30),
8 DTLAST=DTMIN(NPLHAF)
9 M=INTERJ(31)
10 IF(SIGMAX.EQ.0.0)GO TO 240
11 SIGMIN=1./SIGMAX
12 GC TO 244
13 SIGMIN=0.0
14 IF(STIGMIN-7.41*TMINSQ(NPLHAF)) 270,270,250
15 IF(DLAMAX-.079) 255,270,270
16 IF(SIGMIN-.1,1.*TMINSQ(NPLHAF)) 265,260,260
17 IF(DLAMAX-.085) 270,270,265
18 TMINSQ(NPL3HF)=TMINSQ(NPLHAF)
19 GC TO 285
20 IF(DLAMAX-.01) 275,275,280
21 TMINSQ(NPL3HF)=SIGMIN/2.25
22 GC TO 285
280 TMINQ(NPL3HF)=AMINI(SIGMIN/9.00,.005184*TMINSQ(NPLHAF)/DLAMAX**2)
285 DTMIN(NPL3HF)=AMINI(SORT(TMINSQ(NPL3HF)),1.4*DTMIN(NPLHAF))
290 DTMIN(NN)=(DTMIN(NPL3HF)+DTMIN(NPLHAF))/2.
    NP=NPLUSI
    NPLUSI=N
    NPLHAF=NPLUSI
    N=NP
    NMNHAF=N
    NPL3HF=N
    EINSUM=0.
    EKSUM=0.
    USQ(I)=0.(1,N)**2
    DO 300 I=1,IMAX
    EINT(I)=0.
    EKN(I)=0.
    JMAX=INTERJ(I+1)-1
    JMI=INTERJ(I)
    DO 295 J=JMIN,JMAX
    JPLHAF=J
    USQ(I+1)=U(J+1,N)**2
    XI(JPLHAF)=(X(J,N)+X(J+1,N))/2.
    EINT(I)=EINT(I)+E(JPLHAF,N)/HALFRO(I)*HAL FM(JPLHAF)
    EKN(I)=(USQ(I)+USQ(J+1))*HALFM(JPLHAF) +EKN(I)
    EKN(I)=.5*EKN(I)
    EINSUM=EINSUM+EINT(I)
    EKN(6)=.5*EMPROJ*U(JLAST,NMNHAF)**2+EKN(6)
    EKSUM=.5*EMPROJ*U(JLAST,NMNHAF)**2+EKSUM
    EKSUM=EKSUM+EKN(I)
    ESUM=EINSUM+EKSUM
    
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49 WRITE(M,1),K,NUMBER,NDATE1,NDATE2,NDATE3
51 WRITE(M,12)
52 WRITE(M,6) NCYCLE,T,DTLAST,ESUM
53 IF(NCYCLE) 53,53,400
54 DC 57 JPLHAF=1,JLAST1
57 ZMASS(M,2)*HALFM(JPLHAF)
60 WRITE(M,2)
    WRITE(M,3)
    DO 604 L=1,JLAST1
    DO 602 IL=2,ILIMIT
    IF(L=INTERJ{IL}) 602,603,602
602 CONTINUE
    WRITE(M,4) L,X(L,N),U(L,NMNHAF),V(L,N),PPLUSQ(L),Q(L,NMNHAF),
    1E(L,N),AREA(L,N),DTSQ(L),ZMASS(L)
    GC TO 604
603 WRITE(M,5556)
5556 FORMAT(IHO)
    WRITE(M,4) L,X(L,N),U(L,NMNHAF),V(L,N),PPLUSQ(L),Q(L,NMNHAF),
    1E(L,N),AREA(L,N),DTSQ(L),ZMASS(L)
604 CONTINUE
    WRITE(M,4) JLAST,X(JLAST,N),U(JLAST,NMNHAF)
    GC TO 1
400 NYCRAS=HYDRDZ
    IF((NYDRA2.EQ.0).OR.(NYDRA2-60).EQ.0).OR.(NYDRA2-30).EQ.0)
    1 GO TO 100
    IF((NYDRA2.GT.30).AND.(NYDRA2.LT.60)) GO TO 300
    IF(NYDRA2.GT.60) GO TO 600
    NZN=1
    MZM=INTERJ(NYDRA2+1)-1
    GO TO 200
300 NYCRAS=NYDRA2-30
    NZN=INTERJ(NYDRA2)
    MZM=INTERJ(NYDRA2+1)-1
    GC TO 200
600 NYDRA2=NYDRA2-60
    NZN=INTERJ(NYDRA2)
    MZM=JLAST1
    DO 70 JK=NZN,MZM
    JK=JK+NZN+1
    XP6(JKM)=X1(JK)
    VP6(JKM)=U(JK,NMNHAF)/100.
    PP5(JKM)=X1(JK)
    PP5(JKM)=PPLUSQ(JK)
    CCNTINUE
    WRITE(M,7)
    WRITE(M,8)
    WRITE(M,5555)
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100
    
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DO 704 L=1,JLAST1
DO 702 L=2,LIMIT
IF(L=1) TERJ(11) 702,703,702
702 CCINJME 4) L,X(L,N),U(L,NMNHAF),V(L,N),PPLUSQ(L),Q(L,NMNHAF),
WRITE(M,4) L,X(L,N),U(L,NMNHAF),V(L,N),PPLUSQ(L),X1(L)
GC TO 704
703 WRITE(M,5555)
5555 FORMAT(1H,
1E(L,N),AREA(L,N),DTSQ(L),X1(L)
1E(L,N),AREA(L,N),DTSQ(L),X1(L)
704 CONTINUE
WRITE(M,4) JLAST,X(JLAST,N),U(JLAST,NMNHAF)
71 WRITE(M,9)
75 WRITE(M,10) (I,NEQST(I),EKIN(I),EINT(I),I=1,IMAX)
WRITE(M,6) NCYCLE,T,DTLAST,ESUM
5 FORMAT(1H1)
5 IF(ENWRNG) 95,95,80
80 WRITE(M,11)
95 RETURN
99 CONTINUE
40 FORMAT(115,1P,1E13.5)
1 FORMAT(5X,12,20H H V MODEL LAUNCHER,4I3)
2 FCRRAT(118H0, J X(J,N) U(J,N-1/2) V(J+1/2,N) P(J+1/2,N)
1) Q(J+1/2,N-1/2) E(J+1/2,N) AREA(J,N) DTSQ(1/2,1/2) DM(J+1/2)
3 FORMAT(114H CM/MILLISEC CC/CCO GRAMS)
1 BARS
4 FORMAT(14,1P,6E13.5)
6 FCRRAT(15,1P,3E15.5)
7 FORMAT(119H0, J X(J,N) U(J,N-1/2) V(J+1/2,N) P(J+1/2,N)
1) Q(J+1/2,N-1/2) E(J+1/2,N) AREA(J,N) DTSQ(1/2,1/2) X(J+1/2,N)
8 FCRRAT(114H CM/MILLISEC CC/CCO)
9 FORMAT(46HOREGION MATERIAL CM)
10 FCRRAT(15,18, BARS-CC/CCO CM I)
11 FORMAT(15H1, 2E15.5)
12 FORMAT(47HOCYCLE T DT ENERGY CHECK)
END TOTAL E)
SLROUTINE CALCUL (EMLEAD) ENERGY, SPECIFIC VOLUME, AND DENSITY
CCOULTE INITIAL REGIONAL ENERGY, BURST, GMS PRK, GAS SPR, I HEL
COMMON PCON3,SLOPE, RADIUS, CALPGM, T BURST, GMS PRK, GAS SPR, I HEL
COMMON AREA1,DLAMDA2,AREA3,AREA,CQSXC4,CMAXXRT,CS,CQSMAX,CP,CV,DLAMXG
1,DTMIN,DUDT,DLAMDA,DTSQ,DTLAST,DJLAST,DELTA,DELTA,DELTA,DELTA,DELTA,
2DPCMU,DI, DQ2,DS, EZEQ, EINSUM, ESUM, EKSUM, EINT, EKIN, EJETOT, EINTH,
3EWRNG, EI, FORG, GCE, GAMMA, HALFM, HALFRQ, HYDRD, HYDRD3, HYDRAD,
4OUTBDY, QUITD, SKIN, TMAX, TVD1, TVD2, T, TMAX, ROZER, CS, SHPR,
5SSTGMAX, SUSTGMIN, SKIN, TMAX, TVD1, TVD2, T, TMAX, ROZER, CS, SHPR,
6TPRINT, TVNEXT, TMIN3Q, TVREQ, UZZERO, U, USQ, TBAR, TOVRE1, THETA, TWALL,
    
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7 VZERO,V,VOLUME,VISCOS,X,XI,XGRID,XMIN,XMAX,ZMASS,EMPROJ,XSTOP
  COMMON I,MAX,IMU,I,INTERJ,INDX,IL,IMX,I,JPROJ,I,PROJ2,MIN,JMAX,
  1 JPLHAF, JMNHAF, JLAST, JLASTI, JMINI, JMAXI, K, L, P, ACHSQ, NDAT, E1, E2,
  2 NPLHAF, NN, NPL3HF, NP, IQUIT, I, QST, NZONES, NCYCLES, N, NMNHAF, NPLUS1,
  3 NPLHAF, ON, AREA(200,2), CQSQX4(30), JPROJ, JSTOP, R, EMP, TO, A, MOL, DUMVAR
  1 DTMN(3), DLAMDA(200,2), DTSQ(200), DQ1(200), DQ2(200), CV(30), DS(200),
  2 E1(200,2), EINT(30), EKIN(30), FORCE(200), GAMMA(30), NEQST(30),
  3 HALFM(200), HALFR0(30), HYDRAD(200), INTERJ(31), MA, CHSQ(200), ROZ
  4 NZONES(30), OUTBDY(30), PPLUSQ(200), PL(200,2), ROZERR(30),
  5 SKIN(200), USQ(200), I, MINSQ(2), TOVREI(30), TSETA(200), UZERO(30),
  6 U(200,2), VZERR0(30), V(200,2), VISCS(200), X(201,2), XI(200),
  7 ZMASS(200), PO(30), TO(30), AMOL(30), DUMVAR(500,5)
  M=INTERJ(31)
  DO 50 I=1, IMAX
    RCZERO(I)=AMOL(I)/22.4E3
  50 EZERO(I)=R*PO(I)/PO(I)/AMOL(I)*14.5/1.E6*ROZERO(I)
  51 WRTI(EM,21)
  21 FORM(1,1)
  DO 25 IK=1, IMAX
    IF(PO(IK).NE.1.0) GO TO 23
    GAMMA(IK)=1.
  25 EZERO(IK)=1.0
  23 RCZERO(IK)=EMLEAD*453.7/(AREA2*(OUTBDY(2)-OUTBDY(1)))
    IF(PO(IK).NE.2.0) GO TO 24
    GAMMA(IK)=1.
  24 EZERO(IK)=1.0
    IF(EMPIST*453.7/(AREA2*(OUTBDY(3)-OUTBDY(2))))
    GO TO 25
    GAMMA(IK)=1.
  25 EZERO(IK)=0.
    RCZERO(IK)=1.0
    EMPROJ/(AREA3*(OUTBDY(6)-OUTBDY(5)))
  25 CONTINUE
  25 RETURN
END
SUBROUTINE ZEOAB
  ZEROS ALL VARIABLES BETWEEN RUNGS
  COMMON PCON3,SLOPE,RADIUS,CALPGM,TBURND,GMSPOB,GASPRS,IHEL
  1,DTMTN,DUDI,DLAMDA,AREA1,AREA2,AREA3,AREA4,CQXCR,CSQ,CSQMA,BELX,
  2,DPDUM,DQ1,DQ2,DS,EZERO,EINSUM,ESUM,ESUM,EINT,EKIN,EINT,
  3,ELFORCE,GAMMA,HALLFR0,HYDRAD,HYDRAD3,HYDRAD,
  4,OUTBDY,OUTD1,OUTD2,PCON1,PCON2,PPLUSQ,P,PI,Q,ROZERR,SHPR,
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55	SIGMAX,	SIGMIN,	SKIN,TMAX1,	IMAX2,	TVDI1,	TVDI2,	T,IMAX,	TSIGSQ,	TNEXT,	GUNNO709
56	TPRINT,	TVNECUM,	TVNECUM,	X,XI,	XGRID,	XMIN,	XMAX,	ZMMASS,	EMPROJ,XSTOP,	GUNNO710
67	ZERRON,	IMAX1,	INU,	INTERJ,	IMIN,	JLAST1,	JLAST2,	NDATE1,	NDATE2,	GUNNO711
1	JCMNHAF,	JLAF,	JLAF,	JLAF,	JLAF,	JLAF,	JLAF,	JLAF,	JLAF,	GUNNO712
1	JNDLHAF3,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	GUNNO713
3	NPLHAF3,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	GUNNO714
3	NPLHAF3,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	NUMPL3HF,	GUNNO715
1	DIMENS(3),	ALAMDA(200),	DELTA(30),	COSQ(200),	DELTA(30),	COSQ(200),	DELTA(30),	COSQ(200),	DELTA(30),	GUNNO716
2	ZEZER(30),	EMT(30),	EMT(30),	EMT(30),	EMT(30),	EMT(30),	EMT(30),	EMT(30),	EMT(30),	GUNNO717
3	HALFH(200),	HALFRD(30),	HALFRD(30),	HALFRD(30),	HALFRD(30),	HALFRD(30),	HALFRD(30),	HALFRD(30),	HALFRD(30),	GUNNO718
4	HALFH(200),	HALFRD(30),	HALFRD(30),	HALFRD(30),	HALFRD(30),	HALFRD(30),	HALFRD(30),	HALFRD(30),	HALFRD(30),	GUNNO719
5	SKIN(200),	TSIGSQ(200),	TMINSQ(200),	TMINSQ(200),	TMINSQ(200),	TMINSQ(200),	TMINSQ(200),	TMINSQ(200),	TMINSQ(200),	GUNNO720
6	U(20),	USQ(20),	V(20),	V(20),	V(20),	V(20),	V(20),	V(20),	V(20),	GUNNO721
7	ZMASS(200),	PO(30),	TOL(30),	AMOL(30),	AMOL(30),	AMOL(30),	AMOL(30),	AMOL(30),	AMOL(30),	GUNNO722
	CALL ZERO(	AREAS,	AREAS,	AREAS,	AREAS,	AREAS,	AREAS,	AREAS,	AREAS,	GUNNO723
	CALL ZERO(	DUALAS,	DNZNE,	DMU(30),	DPDE,	DPDE,	DPDE,	DPDE,	DPDE,	GUNNO724
	CALL ZERO(	ENTH,	EMRON(30),	PCON(2),	PCON(2),	PCON(2),	PCON(2),	PCON(2),	PCON(2),	GUNNO725
	CALL ZERO(	OUTD12,	PCON(2),	PCON(2),	PCON(2),	PCON(2),	PCON(2),	PCON(2),	PCON(2),	GUNNO726
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO727
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO728
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO729
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO730
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO731
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO732
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO733
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO734
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO735
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO736
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO737
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO738
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO739
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO740
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO741
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO742
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO743
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO744
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO745
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO746
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO747
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO748
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO749
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO750
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO751
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO752
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO753
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO754
	CALL ZERO(	TVAXE2,	YDIA,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	TVI2,	GUNNO755

C C C

52  
54



```

CALL      ZEROB(E,200,2)
CALL      ZEROB(A,EA,200,2)
CALL      ZEROB(Q,200,2)
CALL      ZEROB(U,201,2)
CALL      ZEROB(V,200,2)
CALL      ZEROB(X,200,2)
RETURN
END
C
SUBROUTINE IER0(I1,I2,I3,I4,I5,I6,I7,I8)
ZEROS INTEGERS
I1=0
I2=0
I3=0
I4=0
I5=0
I6=0
I7=0
I8=0
RETURN
END
C
SUBROUTINE ZERO(Z1,Z2,Z3,Z4,Z5,Z6,Z7,Z8)
ZEROS NON-INTEGERS
Z1=0.
Z2=0.
Z3=0.
Z4=0.
Z5=0.
Z6=0.
Z7=0.
Z8=0.
RETURN
END
C
SUBROUTINE ZEROA(IZA,ZA1,ZA2,ZA3,ZA4,ZA5)
ZEROS VECTORS
DIMENSION ZA1(300),ZA2(300),ZA3(300),ZA4(300),ZA5(300)
DO 1 I,ZZ=1, IZA
ZA1(I,ZZ)=0.
ZA2(I,ZZ)=0.
ZA3(I,ZZ)=0.
ZA4(I,ZZ)=0.
ZA5(I,ZZ)=0.
CCONTINUE
1 RETURN
END
C
SUBROUTINE ZEROB(ZAB,IZA,IJB)
ZEROS ARRAYS
DIMENSION ZAB (300,10)

```

GUNNO757  
 GUNNO758  
 GUNNO759  
 GUNNO760  
 GUNNO761  
 GUNNO762  
 GUNNO763  
 GUNNO764  
 GUNNO765  
 GUNNO766  
 GUNNO767  
 GUNNO768  
 GUNNO769  
 GUNNO770  
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 GUNNO797  
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 GUNNO799  
 GUNNO800  
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 GUNNO802  
 GUNNO803  
 GUNNO804









GUNNO853  
 GUNNO854  
 GUNNO855  
 GUNNO856  
 GUNNO857  
 GUNNO858  
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 GUNNO860  
 GUNNO861  
 GUNNO862  
 GUNNO863  
 GUNNO864  
 GUNNO865  
 GUNNO866  
 GUNNO867  
 GUNNO868  
 GUNNO869  
 GUNNO870  
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 GUNNO888  
 GUNNO889  
 GUNNO890  
 GUNNO891  
 GUNNO892  
 GUNNO893  
 GUNNO894  
 GUNNO895  
 GUNNO896  
 GUNNO897  
 GUNNO898  
 GUNNO899  
 GUNNO900

```

I MAX
DO 1 IN=1,
IN20=IN+10
IN30=IN+30
IN40=IN+40
IN50=IN+50
IN60=IN+60
I STORM(IN20)=NEQSI(IN)
I STORM(IN30)=NZONES(IN)
I STORM(IN40)=OUTBDY(IN)
I STORM(IN50)=GAMMA(IN)
I STORM(IN60)=CQSQX4(IN)
I STORM(IN70)=PZERO(IN)
I STORM(IN80)=PO(IN)
I STORM(IN90)=TO(IN)
I STORM(IN100)=AMOL(IN)
I STORM(IN110)=AREAL
I STORM(IN120)=AREA2
I STORM(IN130)=AREA3
I STORM(IN140)=PCON1
I STORM(IN150)=PCON2
I STORM(IN160)=SHPR
I STORM(IN170)=EMPROJ
I STORM(IN180)=OUTDI1
I STORM(IN190)=TMAX1
I STORM(IN200)=OUTDI2
I STORM(IN210)=TMAX2
I STORM(IN220)=XSTOP
I STORM(IN230)=PCON3
I STORM(IN240)=SLOPE
I STORM(IN250)=RADIIUS
I STORM(IN260)=CALPGM
I STORM(IN270)=TURN
I STORM(IN280)=GSPDR
I STORM(IN290)=GASPRS
I STORM(IN300)=R
I STORM(IN310)=MPIST
I STORM(IN320)=PWANT
I STORM(IN330)=PVSLEPE
I STORM(IN340)=XPVI
I STORM(IN350)=XPV2
I STORM(IN360)=PWVERR
I STORM(IN370)=PRESCC
RETURN
END
SUBROUTINE STORE (ISTORM, STORM)
STORAGE ROUTINE
    
```

1

C











```
3 HALFM(200), HALFRO(30), HYDRAD(200), INTERJ(31), MACHSQ(200), NEQST(30)
4 NZONES(30), OUTBDY(30), PPLUSQ(200), P(200,2), Q(200,2), ROZERO(30),
5 XIN(200), T SIGSQ(200), TMINSQ(200), TAVREI(30), THERO(30),
6 U(201,2), USQ(201), VZERO(30), V(200,2), VISCOS(200), X(201,2), X1(200),
7 X2(201,2), X3(201,2), X4(201,2), X5(201,2), X6(201,2), X7(201,2), X8(201,2), X9(201,2), X10(201,2),
8 X11(201,2), X12(201,2), X13(201,2), X14(201,2), X15(201,2), X16(201,2), X17(201,2), X18(201,2), X19(201,2), X20(201,2),
9 X21(201,2), X22(201,2), X23(201,2), X24(201,2), X25(201,2), X26(201,2), X27(201,2), X28(201,2), X29(201,2), X30(201,2),
10 X31(201,2), X32(201,2), X33(201,2), X34(201,2), X35(201,2), X36(201,2), X37(201,2), X38(201,2), X39(201,2), X40(201,2),
11 X41(201,2), X42(201,2), X43(201,2), X44(201,2), X45(201,2), X46(201,2), X47(201,2), X48(201,2), X49(201,2), X50(201,2),
12 X51(201,2), X52(201,2), X53(201,2), X54(201,2), X55(201,2), X56(201,2), X57(201,2), X58(201,2), X59(201,2), X60(201,2),
13 X61(201,2), X62(201,2), X63(201,2), X64(201,2), X65(201,2), X66(201,2), X67(201,2), X68(201,2), X69(201,2), X70(201,2),
14 X71(201,2), X72(201,2), X73(201,2), X74(201,2), X75(201,2), X76(201,2), X77(201,2), X78(201,2), X79(201,2), X80(201,2),
15 X81(201,2), X82(201,2), X83(201,2), X84(201,2), X85(201,2), X86(201,2), X87(201,2), X88(201,2), X89(201,2), X90(201,2),
16 X91(201,2), X92(201,2), X93(201,2), X94(201,2), X95(201,2), X96(201,2), X97(201,2), X98(201,2), X99(201,2), X100(201,2),
17 X101(201,2), X102(201,2), X103(201,2), X104(201,2), X105(201,2), X106(201,2), X107(201,2), X108(201,2), X109(201,2), X110(201,2),
18 X111(201,2), X112(201,2), X113(201,2), X114(201,2), X115(201,2), X116(201,2), X117(201,2), X118(201,2), X119(201,2), X120(201,2),
19 X121(201,2), X122(201,2), X123(201,2), X124(201,2), X125(201,2), X126(201,2), X127(201,2), X128(201,2), X129(201,2), X130(201,2),
20 X131(201,2), X132(201,2), X133(201,2), X134(201,2), X135(201,2), X136(201,2), X137(201,2), X138(201,2), X139(201,2), X140(201,2),
21 X141(201,2), X142(201,2), X143(201,2), X144(201,2), X145(201,2), X146(201,2), X147(201,2), X148(201,2), X149(201,2), X150(201,2),
22 X151(201,2), X152(201,2), X153(201,2), X154(201,2), X155(201,2), X156(201,2), X157(201,2), X158(201,2), X159(201,2), X160(201,2),
23 X161(201,2), X162(201,2), X163(201,2), X164(201,2), X165(201,2), X166(201,2), X167(201,2), X168(201,2), X169(201,2), X170(201,2),
24 X171(201,2), X172(201,2), X173(201,2), X174(201,2), X175(201,2), X176(201,2), X177(201,2), X178(201,2), X179(201,2), X180(201,2),
25 X181(201,2), X182(201,2), X183(201,2), X184(201,2), X185(201,2), X186(201,2), X187(201,2), X188(201,2), X189(201,2), X190(201,2),
26 X191(201,2), X192(201,2), X193(201,2), X194(201,2), X195(201,2), X196(201,2), X197(201,2), X198(201,2), X199(201,2), X200(201,2),
27 X201(201,2), X202(201,2), X203(201,2), X204(201,2), X205(201,2), X206(201,2), X207(201,2), X208(201,2), X209(201,2), X210(201,2),
28 X211(201,2), X212(201,2), X213(201,2), X214(201,2), X215(201,2), X216(201,2), X217(201,2), X218(201,2), X219(201,2), X220(201,2),
29 X221(201,2), X222(201,2), X223(201,2), X224(201,2), X225(201,2), X226(201,2), X227(201,2), X228(201,2), X229(201,2), X230(201,2),
30 X231(201,2), X232(201,2), X233(201,2), X234(201,2), X235(201,2), X236(201,2), X237(201,2), X238(201,2), X239(201,2), X240(201,2),
31 X241(201,2), X242(201,2), X243(201,2), X244(201,2), X245(201,2), X246(201,2), X247(201,2), X248(201,2), X249(201,2), X250(201,2),
32 X251(201,2), X252(201,2), X253(201,2), X254(201,2), X255(201,2), X256(201,2), X257(201,2), X258(201,2), X259(201,2), X260(201,2),
33 X261(201,2), X262(201,2), X263(201,2), X264(201,2), X265(201,2), X266(201,2), X267(201,2), X268(201,2), X269(201,2), X270(201,2),
34 X271(201,2), X272(201,2), X273(201,2), X274(201,2), X275(201,2), X276(201,2), X277(201,2), X278(201,2), X279(201,2), X280(201,2),
35 HALFR0(I)=ROZERO(I)/2.
INTERJ(I)=I
DO 40 I=1,IMAX
INTERJ(I+1)=INTERJ(I)+NZONES(I)
JLAST=INTERJ(IMAX+1)
JLAST1=JLAST-1
DO 45 I=1,JLAST1
JLAST2=JLAST1
DNZCNE=NZONES(I)
DELX(I)=OUTBDY(I)/DNZONE
X(I,N)=0.
U(I,NMNHAF)=UZERO(I)
DNZONE=NZONES(I)
DELX(I)=OUTBDY(I)-OUTBDY(I-1)/DNZONE
DO 55 I=1,IMAX
JMIN=INTERJ(I)+1
JMAX=INTERJ(I+1)-1
DC 50 J=JMIN,JMAX
JMNHAF=J-1
U(J,NMNHAF)=UZERO(I)
V(J,NMNHAF,N)=VZERO(I)
E(JMNHAF,N)=EZERO(I)
X(J,N)=X(J-1,N)+DELX(I)
X(JMAX+1,N)=OUTBDY(I)
U(JMAX+1,NMNHAF)=UZERO(I)
E(JMAX,N)=EZERO(I)
V(JMAX,N)=VZERO(I)
DO 132 J=1,JLAST
DO 130 I=1,IMAX
JMIN=INTERJ(I)+1
JMAX=INTERJ(I+1)
DC 125 J=JMIN,JMAX
JMNHAF=J-1
CALL VCOMP
P=HALFM(JMNHAF)=HALFR0(I)/V(JMNHAF,N)*VOLVOLUME
CCNTINUE
HALFM(JLAST)=HALFM(JLAST)+EMPROJ
INDEX=NEQST(I)
IF(INDEX.EQ.1)CALL EGST1
IF(INDEX.EQ.2)CALL EGST2
```





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130 IF(INDEX.EQ.3)CALL EQST3
CONTINUE
135 JMNHAF=1,JLAST1
150 PPLUSQ(JMNHAF)=P(JMNHAF,N)
DKI=1
DKI=2,=0.
EINSUM=0.
EKSUM=0.
ETOT=0.
USQ(I)=U(I,N)**2
DO 165 I=1,IMAX
EINT(I)=0.
EKIN(I)=0.
JMIN=INTERJ(I)
JMAX=INTERJ(I+1)-1
CC 160 J=JMIN,JMAX
JPLHAF=J
EINT(J+1)=U(J+1,N)**2
EINT(I)=EINT(J)+E(JPLHAF,N)/HALFRO(I)*HALFM(JPLHAF)*DK
160 EKIN(I)=(USQ(J)+USQ(J+1))*HALFM(JPLHAF)*DK+EKIN(I)
EINSUM=EINSUM+EINT(I)
EKSUM=EKSUM+EKIN(I)
ETOT=ETOT+EINSUM+EKSUM
ESUM=ETOT*ETOT
ETENTH=.125*(X(JMAX,N)-X(1,N))
175 XGRID=.125*(X(JMAX,N)-X(1,N))
XMIN=X(1,N)-XGRID
XMAX=X(JMAX,N)+XGRID
180 CALL OUTPUT
RETURN
END
SUBROUTINE DYNMEQ
CALCULATES MASS POINT VELOCITY AND ZONE SPECIFIC VOLUME AND
BCONDARIES
CCCOMMON PCON3,SLOPE,RADIUS,CALPGM,TBURND,GMSFDR,GASPRS,IHEL
CCCOMMON ARE1,AREA2,AREA3,AREA,CQSQX4,CMAXR,CSCQ,CSQMAX,CP,CV,DLAMAX,
1,DTMTN,DUT,DIAMDA,DISQ,DLAST,DJLAST,DEKIN,DELX,DMU,DPDE,
2,DTCMU,QI,DO2,DS,EZERO,EINSUM,ESUM,EKIN,EINT,ETOT,ETENTH,
3EWRONG,EL,FORCE,GAMMA,HALFM,HALFRD,HYDRD,HYDRD3,HYDRAD,
4OUTBDY,OUTDT1,OUTDT2,PCON2,PPLUSQ,PPI,QR,ZERO,SHPR,
5SIGMAX,SIGMIN,SKIN,MAX,TVDI,VDT2,TMAX,TSCOT,XTNEXT,
6VPRINI,TVNEQ,MINSCQ,TVPREQ,UZERO,UUSQ,TBAR,TVREI,THEAT,ITWALL,
7VZONAV,VOLUME,VISCOS,X,XI,INDE,X,ININT,INU,I,INPROJ2,JMIN,JMAX,J,
CCCOMMON IMAX,JLAST,JMIN,JMAX,K,L,MACHSQ,NDATE1,NDATE2,
1JPLHAF,JMNHAF,N,NCHKE,NEQST,NZONES,NPLUSI,
2NDATE3,NUMBER,NTV,NPL3HF,NP,IQUIT,JPROJ,JSTOP,R,EMPIST,PO,TO,AMOL,DUMVAR
3NPLHAF,NN,NPL3HF,NP,IQUIT,JPROJ,JSTOP,R,EMPIST,PO,TO,AMOL,DUMVAR

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C C



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DIMENSION AREA(200,2),CQSQX4(30),CMAXR(30),CSQ(200),CP(30),CV(30),GUNN1093
1DTMIN(30),DLAMD(20),DTSQ(200),DELX(30),DQ1(200),DQ2(200),DS(200),GUNN1094
2VZRO(200),EINT(30),EKN(30),EKN(30),FORCE(200),GAMMA(30),GUNN1095
3HALFM(200),HALFBY(30),HYDRA(200),INTERJ(30),MACHSQ(200),NEQST(30),GUNN1096
4NZNONES(30),OULBQ(30),PPLUSQ(200),P(200,2),Q(200,2),ROZERO(30),GUNN1097
5KIN(200),SIGSQ(200),TMINSQ(200),VZREI(200),HETA(200),UZERO(30),GUNN1098
6U(201,2),USQ(201),VZERO(30),V(200,2),VISCDS(200),X(201,2),X1(200),GUNN1099
7ZMASS(200),PO(30),TD(30),AMDL(30),DUMVAR(500,5)
GUNN1100
C 120 CCNTINUE
120 I=1
120 DTMAX=0.
125 STGMAX=0.
S=T+DTMIN(NPLHAF)
N=CYLE=NYCLE+1
DO 245 I=1,IMAX
150 DO 245 I=1,IMAX
NZN=NZNONES(I+1)
CMAXR(I)=0.
CSCMAX=0.
JMIN=INTERJ(I)+1
JMAX=INTERJ(I+1)
DO 230 J=JMIN,JMAX
JPLHAF=J
JMNHAF=J-1
IF(JLAST-I) 155,155,1700
361 DUDT=PPLUSQ(JMNHAF)*AREA(JLAST,N)/HALFM(JMNHAF)
155 IF(JPROJ.EQ.300.AND.E(JMNHAF,N).NE.0.0) GC TO 195
GO TO 901
1700 IF(JPROJ.EQ.300) GO TO 1755
IF(J.EQ.INTERJ(6)) GO TO 901
IF(J.EQ.INTERJ(6)) GO TO 902
GC TO 1755
901 IF(PPLUSQ(JMNHAF)-SHPR) 902,903,903
902 U(J,NPLHAF)=0.0
GC TO 196
903 JPROJ=500
1755 DTSQ(200)=T
IF(J.EQ.JMAX.AND.NZN.EQ.1) GO TO 876
IF(J.EQ.JMAX.AND.NZN.GT.1) GO TO 800
DUDT=(PPLUSQ(JMNHAF)-PPLUSQ(JPLHAF))*AREA(J,N)/(HALFM(JMNHAF)+
1HALFM(JPLHAF))
GC TO 195
800 IF(J.EQ.INTERJ(6)) GO TO 863
DUDT=-((1.5*(PPLUSQ(JPLHAF)-PPLUSQ(JMNHAF))-(PPLUSQ(JPLHAF+1)-
1PPLUSQ(JMNHAF-1))/6.)*AREA(J,N)/(HALFM(JMNHAF)+HALFM(JPLHAF))
GC TO 195
863 DUDT=-((1.5*(PPLUSQ(JPLHAF)-PPLUSQ(JMNHAF))-(PPLUSQ(JPLHAF+1)-
1PPLUSQ(JMNHAF-1))/73.+2.*PPLUSQ(JMNHAF-1))/73.)*
11/76.)*AREA(J,N)/(HALFM(JMNHAF)+HALFM(JPLHAF))
GUNN1101
GUNN1102
GUNN1103
GUNN1104
GUNN1105
GUNN1106
GUNN1107
GUNN1108
GUNN1109
GUNN1110
GUNN1111
GUNN1112
GUNN1113
GUNN1114
GUNN1115
GUNN1116
GUNN1117
GUNN1118
GUNN1119
GUNN1120
GUNN1121
GUNN1122
GUNN1123
GUNN1124
GUNN1125
GUNN1126
GUNN1127
GUNN1128
GUNN1129
GUNN1130
GUNN1131
GUNN1132
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GUNN1134
GUNN1135
GUNN1136
GUNN1137
GUNN1138
GUNN1139
GUNN1140
    
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154 IF(IT-GE,(DTSQ(200)+DTSQ(199))) GO TO 194
    DUDT=DUDT*(1-DTSQ(200))/DTSQ(199)
    CONTINUE
    GO TO 155
876 A=2.*HALFM(JMNHAF)+HALFM(JPLHAF)
    B=HALFM(JMNHAF)+HALFM(JPLHAF)
    DUDT=(12.*A**2*PPPLUSQ(JLNMHAF)
    1-(2.*A-B)*(A+B)*PPPLUSQ(LNMHAF)
    2+(A-B)*B*PPPLUSQ(JMNHAF-1))/((A*(A+B)*B)*DUDT)
155 U(J,NPLHAF)=U(J,NMNHAF)+DTMIN(NN)*DUDT
156 X(J,NPLUS1)=X(J,N)+DTMIN(NPLHAF)*U(J,NPLHAF)
    CALL ARCOMP
    V(JMNHAF,NPLUS1)=HALFRO(I)/HALFM(JMNHAF)*VOLUME
200 IF(U(J,NPLHAF)-U(J-1,NPLHAF)) 205,225,225
205 Q(JMNHAF,NPLHAF)=CSQX4(I)*HALFRO(I)*U(J,NPLHAF)-U(J-1,NPLHAF))
    1*Q2/(V(JMNHAF,NPLUS1)+V(JMNHAF,N))
    GO TO 230
225 Q(JMNHAF,NPLHAF)=0.
230 CONTINUE
    INDEX=NEQST(I)
    IF(INDEX.EQ.1)CALL ECST1
    IF(INDEX.EQ.2)CALL ECST2
    IF(INDEX.EQ.3)CALL ECST3
53 DO 240 J=JMIN,JMAX
    JMNHAF=J-1
    IF(JPROJ.LT.300.AND.J.GT.INTERJ(6)) GO TO 24
    TSIGSQ(JMNHAF)=CSQ(JMNHAF)/(X(J,NPLUS1)-X(J-1,NPLUS1))*2
24 CONTINUE
    PPLUSQ(JMNHAF)=P(JMNHAF,NPLUS1)+Q(JMNHAF,NPLHAF)
    DLAMDA(JMNHAF)=CSQX4(I)/2.*(V(JMNHAF,N
    1(V(JMNHAF,N)+V(JMNHAF,NPLUS1))
    CFANGED TO MAX1 JANDUARY 16, 1967 DKS
    DLAMAX=MAX1(DLAMDA(JMNHAF),DLAMAX)
    SIGMAX=MAX1(TSIGSQ(JMNHAF),SIGMAX)
    CSQMAX=MAX1(CSQMAX,CSQ(JMNHAF))
    IF(TSIGSQ(JMNHAF).NE.0.0) GO TO 240
    DLSQ(JMNHAF)=0.0
    CL TO 245
240 DTSQ(JMNHAF)=111111/TSIGSQ(JMNHAF)
245 CMXR(I)=SORT(CSQMAX)
340 CONTINUE
346 RETURN
END
C
SUBROUTINE AKCOMP
    DEFINES ZONE CROSS SECTIONAL AREA
    COMMON PCOM3,SLOPE,RADIUS,CALPGM,TBURND,GMSFDR,GASPRS,IHEL
    COMMON AREA1,AREA2,AREA3,AREA,CSQX4,CMA XR,CSQ,CSQMAX,CP,CV,DLAMAX,GUNN1187
    GUNN1141
    GUNN1142
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    GUNN1177
    GUNN1178
    GUNN1179
    GUNN1180
    GUNN1181
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    GUNN1183
    GUNN1184
    GUNN1185
    GUNN1186
    GUNN1187
    GUNN1188
    
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2 EZERO(30), F(200,2), EINT(30), EKin(30), FORCE(200), GAMMA(30), NEGST(30)
3 FALRM(200), HALFRQ(30), HYDRAD(200), INTERJ(31), MACHSQ(200), NEGST(30)
4 NZONES(30), OUTBDY(30), PPLUSQ(200), P(200,2), Q(200,2), ROZERO(30),
5 SKIN(200), TSIGSQ(200), TMINSQ(200), TOVREL(200), THETA(200), UZERO(30),
6 U(201,2), USQ(201), VZERO(30), V(200,2), VISCCSQ(200), X(201,2), X1(200),
7 MASS(200), PD(30), TD(30), AMOL(30), DUMVAR(500,5)
8 X(201,0)
9 XPVZ=0.
10 PVEKRG=0.
11 PRES CG=0.
12 IF(X(J,NPLUS1)-PCON1) 3,3,4
13 GO TO 17
14 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA1
15 IF(X(J,NPLUS1)-PCON1) 5,5,8
16 IF(X(J-1,NPLUS1)-PCON1) 6,7
17 VOLUME=(X(J,NPLUS1)-PCON1)*AREA2+(PCON1-X(J-1,NPLUS1))*AREA1
18 GO TO 17
19 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA2
20 GO TO 17
21 IF(X(J,NPLUS1)-PCON2) 9,9,12
22 IF(X(J-1,NPLUS1)-PCON2) 10,11,11
23 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA2
24 GO TO 17
25 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA2
26 GO TO 17
27 IF(X(J-1,NPLUS1)-PCON3) 14,13,13
28 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA3
29 GO TO 17
30 IF(X(J-1,NPLUS1)-PCON2) 16,15,15
31 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA3
32 GO TO 17
33 VOLUME=(X(J,NPLUS1)-X(J-1,NPLUS1))*AREA3
34 RETURN
35 END
36 SUBROUTINE EQST1
37 CALCULATE PRESSURE AND ENERGY FOR IDEAL GAS ZONES
38 COMMON PCOM3, SLOPE, RAD1US, CALPGM, TBOURND, GAS, QMA X, CP, CV, DLAMAX,
39 COMMON AREA1, AREA2, AREA3, AREA4, CQS, QX4, CMA XR, S, CSQ, QMA X, DEL X, CMU, DPDE,
40 DTMIN, DUDT, DLAMDA, DTSC, ELAST, DLAST, DJLAST, DNZONE, DEL X, ETOI, STENTH,
41 PDCMU, DGL, O2DS, EZERO, EINSUM, ESUM, EKSUM, EKIN, HYDRD2, HYDRD3, HYDRAD,
42 FORTONG, EL, FORCE, GAMMA, HALFR, HALFRQ, P, PI, Q, ROZ, HZCR, SHPR,
43 OUTBDY, OUTDT1, OUTDT2, PCON1, MAX1, TVD1, TVD2, TVD12, TVD12, TMAX, TSIGSQ, TMIN,
44 STPRNG, STVNET, TMIN, SKIN, TMAX1, TMAX2, TMIN, TVD1, TVD2, TVD12, TMAX, TSIGSQ, TMIN,
45 TPRNG, V, VOLUME, VISCOS, TVF, E, U, ZERO, U, USQ, TVD1, TVD2, TVD12, TMAX, TSIGSQ, TMIN,
46 VZERO, V, VOLUME, VISCOS, TVF, E, U, ZERO, U, USQ, TVD1, TVD2, TVD12, TMAX, TSIGSQ, TMIN,
47 JPCOM, IMAX1, INU, I, I, INTERJ, INDEX, IL, IMIT, J, K, L, JPROJ, J, JMIN, JMAX, J,
48 JPHAF, JLAST, JLAST, JMINI, JMAX1, J, K, L, JPROJ, J, JMIN, JMAX, J,
49 NCDATE3, NUMBER, NTV, NCHEKE, NEGST, NZONES, NCYCLE, N, NMINHAF, NPLUS1,

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C



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3 NPLHAF, NN, NPREA(200,2), IQUIT, JPROJ, JSTOP,R, EMP IST, PO, TO, AMOL, DUMVAR, GUNN1285
DIMENSION AREA(200,2), CQSQ(200,1), CMAX(30), CEX4(30), CSQ(200,1), CP(30), CV(30), GUNN1286
1DTRIN(30), DLAMDA(200), DTSQ(200), DELX(30), DQ1(200), DQ2(200), DQ3(200), DS(200), GUNN1287
2ZEZER(200), E(200,2), ENT(30), EKIN(30), EOR(200), GAMMA(30), GUNN1288
3HALFML(200), HALFRO(30), HYDRAD(200), INTERJ(31), MACHSQ(200), NEQST(30), GUNN1289
4 NZONES(30), OUTBDY(30), PPLUSQ(200), PL(200,2), Q(200,2), ROZERO(30), GUNN1290
5 SKIN(200), TSI(200), TMINSQ(200), TOVRE(30), THETA(200), UZERO(30), GUNN1291
6 U(200,2), USQ(200), VZE(200), V(200,2), VISCOS(200), X(201,2), X1(200), GUNN1292
7 ZMASS(200), POL(30), TOI(30), AMOL(30), DUMVAR(500,5) GUNN1293
JMAX1=JMIN-1 GUNN1294
JMAX1=JMAX-1 GUNN1295
DO 10 JMNHAF, N) GUNN1296
10 JMNHAF, N) -(P(JMNHAF, N)+Q(JMNHAF, NPLHAF))*(V(JMNHAF, NPLUS1)- GUNN1297
1V(JMNHAF, N)) GUNN1298
PL=EI*(GAMMA(I)-1.0)/V(JMNHAF, NPLUS1) GUNN1299
E(JMNHAF, N) GUNN1300
P(JMNHAF, N) GUNN1301
1V(JMNHAF, N) US1)=E(JMNHAF, NPLUS1)*(GAMMA(I)-1.0)/V(JMNHAF, NPLUS1) GUNN1302
CSQ(JMNHAF)=GAMMA(I)*(GAMMA(I)-1.0)*E(JMNHAF, NPLUS1)/RZERO(I) GUNN1303
RETURN GUNN1304
END GUNN1305
SUBROUTINE EQST2 GUNN1306
CALCULATE PRESSURE AND ENERGY FOR NON-IDEAL GAS ZONES GUNN1307
COMMON PCOIN3, AREA2, AREA3, AREA4, DTG, DTLAST, EOR, CSQMAX, CP, CV, DLAMDA, GUNN1308
1 DTRIN, DUDT, DIAMDA, DTG, DTLAST, EOR, CSQMAX, CP, CV, DLAMDA, GUNN1309
2 PDMAU, FGL, DQZDS, EZER, GAMMA, HALFM, HALFR, HDRI, HPI, QROZER, S, HPR, GUNN1310
3 WRONG, E, E1, FOUT, J, OUTD, J2, PCON1, PCON2, PPLUSQ, P, PI, QROZER, S, HPR, GUNN1311
40UTRO, OUTD, J, OUTD, J2, PCON1, PCON2, PPLUSQ, P, PI, QROZER, S, HPR, GUNN1312
5 SIGMA, SIGMIN, SKIN, TMAX1, TMAX2, TVD1, TVD2, TVT, TMAX, TSI, CSQ, TNEXT, GUNN1313
6 TPRINT, TVNEXT, TMINSQ, TVFREQ, UZER, U, USQ, TBAR, TOVRE1, THETA, TWALL, GUNN1314
7 VZERO, VOLUME, VISCOS, X, X1, XGRD, XMIN, XMAX, ZMASS, EMPROJ, X, XSTOP, GUNN1315
COMMON I, MAX, INU, I, INTERJ, INDEX, I, J, K, L, MACHSQ, NDAT1, NDAT2, GUNN1316
1 JPLHAF, JMNHAF, JLAST, JLAST, JMIN, JMAX, J, K, L, MACHSQ, NDAT1, NDAT2, GUNN1317
2 NDAT3, NUMBER, NT, V, NCHKE, NEQST, NZONES, NCYCLE, NZ, NMNHF, NPLUS1, GUNN1318
3 NPLHAF, NN, NPREA(200,2), IQUIT, JPROJ, JSTOP,R, EMP IST, PO, TO, AMOL, DUMVAR, GUNN1319
DIMENSION AREA(200,2), CQSQ(200,1), CMAX(30), CEX4(30), CSQ(200,1), CP(30), CV(30), GUNN1320
1DTRIN(30), DLAMDA(200), DTSQ(200), DELX(30), DQ1(200), DQ2(200), DQ3(200), GUNN1321
2ZEZER(30), E(200,2), ENT(30), EKIN(30), EOR(200), GAMMA(30), GUNN1322
3HALFML(200), HALFRO(30), HYDRAD(200), INTERJ(31), MACHSQ(200), NEQST(30), GUNN1323
4 NZONES(30), OUTBDY(30), PPLUSQ(200), PL(200,2), Q(200,2), ROZERO(30), GUNN1324
5 SKIN(200), TSI(200), TMINSQ(200), TOVRE(30), THETA(200), UZERO(30), GUNN1325
6 U(200,2), USQ(200), VZE(200), V(200,2), VISCOS(200), X(201,2), X1(200), GUNN1326
7 ZMASS(200), POL(30), TOI(30), AMOL(30), DUMVAR(500,5) GUNN1327
IF(NCYCLE.EQ.0) GO TO 3 GUNN1328
IF(NCYCLE.EQ.1) GO TO 3 GUNN1329
IF(NCYCLE.EQ.2) GO TO 3 GUNN1330
IF(INTERJ(30))13,1,3 GUNN1331
1 NCHEKE=0 GUNN1332

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GUNN1380

IBURND=0
TOLD=0.
INTERJ(30)=2
ZMAS(200)=2
GASPRS=CASPR*14.5
PVOL=GMSPR/AREA1*.001-PVOL
GMOLES=GASPRS*GVOL/24.61
PMOLES=GMSPR/25.
PRESUR=(GMOLES+PMOLES)*24.61/(GVOL+PVOL)*1.0138
35 GAMMA(I)=(GMOLES*1.667+PMOLES*1.23)/(GMOLES+PMOLES)
    WGTMOL=(GMOLES*4.0026+PMOLES*25.0)/(GMOLES+PMOLES)
    GO TO 50
40 GAMMA(I)=(GMOLES*1.4+PMOLES*1.23)/(GMOLES+PMOLES)
    WGTMOL=(GMOLES*2.0+PMOLES*25.0)/(GMOLES+PMOLES)
50 SPCVOL=83.17*300.0/(PRESUR*WGTMOL)
    RZERO(I)=SPCVOL*RZERO(I)
    EZERO(I)=PRESUR*VZERO(I)/(GAMMA(I)-1.0)
    JMINI=JMIN-1
    JMAXI=JMAX-1
    DO 20 J=MINI,JMAXI
    E(J,N)=EZERO(I)
20 EPEAK=CALPGM*41.84*RZERO(I)*PMOLES*25.0/(PMOLES*25.0+GMOLES*2.0)
    HALFR(I)=RZERO(I)/2.
    DC 30 J=JMIN,JMAX
    VOLUME=(X(J,N)-X(J-1,N))*AREAL
30 HALF(J-1)=HALFR(I)/V(J-1,N)*VOLUME
    3 JMINI=JMIN-1
    JMAXI=JMAX-1
    IF(TBURND)4,4,7
4 IF(TBURND).EQ.0.0 GO TO 6
    C STATEMENT IF(TBURND.EQ.0.0) GO TO 6 WAS INSERTED DURING CON-
    C VERSION TO THE G.E. 635
5 DEL=EPEAK*(T-TOLD)/TBURND
    TOLD=T
6 DEL=0.
7 IBURND=1
    EI=E(JMNHAF,N)-(P(JMNHAF,N)+Q(JMNHAF,NPLHAF))* (V(JMNHAF,NPLUS1)-
    1V(JMNHAF,N))+DEL
    PI=(GAMMA(I)-1.0)*EI/V(JMNHAF,NPLUS1)
    E(JMNHAF,NPLUS1)=EI-.5*(PI-P(JMNHAF,N))* (V(JMNHAF,NPLUS1)-
    1V(JMNHAF,N))

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10 P(JMNHAF,NPLUS1)={GAMMA(I)-1.}*E(JMNHAF,NPLUS1)/V(JMNHAF,NPLUS1)
   CSQ(JMNHAF)=GAMMA(I)*{GAMMA(I)-1.}*E(JMNHAF,NPLUS1)/ROZERO(I)
   RETURN
END
SUBROUTINE EQST3
CALCULATE PRESSURE AND ENERGY FOR SOLID ZONES
CALCULATE RADIUS, TBOURND, GMSDDR, GASPRS, IHEL, V, DLAMAX
COMMON AREA1, AREA2, AREA3, AREA4, CQSQ, CTI, CMAXR, CSO, CSQW, CX, CP, CMU, DPDE,
1, DTMIN, DDU1, DLAMDA, DTSG, DLAST, DJLAST, DJLST, DNZONE, DELX, DELY, ELENTH,
2PDRONG, DQ1, DQ2, DS, GAMMA, HALFM, HALFR, HYDRD1, HYDRD2, HYDRD3, HPR,
3EWRONG, EL, FORCE, GAMMA, INSUM, LFRORDR, P, P1, Q, ROZ, SHPR,
4OUTOT1, OUTOT2, PCON1, PCGN2, PPLUSQ, P, P1, Q, ROZ, SHPR,
5SIGMAX, SIGMIN, SKINSG, TVFRSQ, UZERRO, U, USQ, TBAR, TVR, TVDT2, TMAX, TSI, TSGSQ, T, TNEXT,
6VZERO, V, VOL, VOLUME, V, VISCOS, X, XI, XGRID, XMIN, XMAX, XMASS, EMPROJ, X, XTOP,
7TPRINT, T, MAX, INU, I, INTERJ, IINDEX, ILIMIT, JPROJ, J, JPROJ2, JMIN, JMAX, J,
COMMON JMNHAF, JMHAF, JLA, JLA2, JLA3, JLA4, JLA5, JLA6, JLA7, JLA8, JLA9, JLA10,
1JPLHAF, JMHAF, NIV, NCHEKE, NEST, NZONES, KCYCL, K, L, LACHSO, NDATEL, NDATE2,
2NDATE3, NUMBER, NIV, NCHEKE, NEST, NZONES, KCYCL, K, L, LACHSO, NDATEL, NDATE2,
3NPLHAF, NN, NPL3HF, NP, IQUIT, JPROJ, JSTOP, R, EMP, ST, PO, TO, AMOL, DUMVAR
4DIMENSION AREA4(200), DTSG(200), DELX(30), CMAXR(30), USQ(200), CP(30), LCV(30),
1DZERO(30), EA(200,2), EINT(30), EKIN(30), FORCE(200), DQ1(200), DQ2(200),
2EZERO(200), HALFR(30), HYDRAD(200), INTERJ(31), MACHSQ(200), GAMMA(30),
3HALFM(200), OUTBDY(30), PPLUSQ(200), P(200,2), Q(200,2), ROZERO(30),
4EKNIN(200), TSI(30), TMINSG(200), TMINSG(2), TVR(30), THTA(30), UZERRO(30),
5U(200,2), USQ(201), VZERO(30), V(200,2), VISCOS(200), X(201,2), XI(200),
6U(200,2), USQ(201), VZERO(30), V(200,2), DUMVAR(500,5)
7ZMAS(200), P(30), TO(30), AMOL(30)
JMNI=JMNI-1
JMAXI=JMAXI-1
DO 10 JMNHAF=JMNI, JMAXI
  CMU=1./V(JMNHAF,NPLUS1)-1.
  E1=E(JMNHAF,N) - {P(JMNHAF,N) + Q(JMNHAF,NPLHAF)} * (V(JMNHAF,NPLUS1) -
1V(JMNHAF,N))
  DFDU=21297.0*(DMU+1.0)**6-3041.4
  P(JMNHAF,NPLUS1)=3042.4*(DMU+1.0)**7-3041.4
  IF(P(JMNHAF,NPLUS1)>5000.0) 9,11,11
5 P(JMNHAF,NPLUS1)=-3000.
  E(JMNHAF,NPLUS1)=E1-.5*(P(JMNHAF,NPLUS1)-P(JMNHAF,N)) * (V(JMNHAF,
11 NPLUS1)-V(JMNHAF,N))
  CSQ(JMNHAF)=DPDMU/ROZERO(I)
  RETURN
END
SUBROUTINE PVCHNG (PVW, ERR, VEL, PLOAD, GAS, AVEL, ALOAD, AGAS, NU)
DIMENSION GAS(30), AVEL(100), ALOAD(100), AGAS(100)
PVLO = 10
PVHI = 5000.
DO 20 N = 1, NU
  IF (AGAS(N).NE.GAS(3)) GO TO 20

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IF (ABS(AVEL(N)-PVW).LT.ERR) GO TO 30
IF (AVEL(N).GT.PVW.AND.AVEL(N).GT.PVHI) GO TO 20
IF (AVEL(N).LT.PVW.AND.AVEL(N).LT.PVLO) GO TO 20
IF (AVEL(N).LT.PVW) GO TO 40
HLOAD=ALOAD(N)
PVHI = AVEL (N)
GO TO 20
40 BALOAD = ALOAD (N)
PVLO = AVEL (N)
20 CONTINUE
IF(PVLG.EQ.10.0.OR.PVHI.EQ.5000.) GO TO 60
PLOAD=BALOAD*(PVW-PVLO)*(BALOAD-HLOAD)/(PVLO-PVHI)
GC TO 50
30 PLGAD=ALOAD(N)
GO TO 50
60 PLOAD= FLOAD +(PVW-VEL) * 20.
50 GAS(TA)=PLOAD
RETURN
END
    
```



INPUT FORMAT

CARD 1 (4I3,F10.0)  
IDATA = 0, STANDARD 18 CARD INPUT  
= NAMELIST INPUT OF ALL VARIABLES ON CARDS  
IPRNTZ = 0, STANDARD RUN  
= 1, PRINT OUT INITIAL DATA ONLY  
INTRNSF = 0, USE DISK SCRATCH FILE AND PRINT OUT ONLY LAST PISTON ITERATION  
= 1, PRINT OUT ALL PISTON ITERATIONS (HYPERVELOCITY MODEL ONLY)  
IPUNCH = 0, NO PUNCHED OUTPUT  
= 1, PUNCHED OUTPUT OF MODEL BASE PRESSURE VS TIME  
DTSQ(199) FINITE BREAK VALVE OPENING TIME

CARD 2 (20I3)  
IMAX = NUMBER OF REGIONS (UP TO SIX)  
NDATE1 = MONTH  
NDATE2 = DAY  
NDATE3 = YEAR  
NUMBER = RUN IDENTIFICATION NUMBER  
NCHEKE = 0, NO ENERGY CHECK  
= 1, ENERGY MONITORED AND PROBLEM STOPPED IF THE TOTAL ENERGY  
INU = 0, ALL ZONES HAVE ZERO INITIAL VELOCITY  
= 1, ALLOWS INITIAL VELOCITY FOR EACH ZONE TO BE READ  
JPROJ = MASS POINT NUMBER OF PROJECTILE



- CARD 3 (20I3)  
NEQST(I) = NUMBER OR INDEX OF EQUATION OF STATE USED IN REGION I
- CARD 4 (20I3)  
NZONES(I) = NUMBER OF ZONES IN REGION I
- CARD 5 (7F10.0)  
OUTBDY(I) = DISTANCE IN CM TO OUTER INTERFACE OF REGION I
- CARD 6 (7F10.0)  
GAMMA(I) = RATION OF SPECIFIC HEATS FOR REGION I
- CARD 7 (7F10.0)  
CQSQX4(I) = CONSTANT USED IN ARTIFICIAL VISCOSITY COMPUTATION  
(GOOD VALUES ARE 4.0 FOR GAS REGION, 9.0 FOR SOLID REGION)
- CARD 8 (7F10.0)  
AREA1 = AREA IN SQ CM OF FIRST CONSTANT AREA SECTION (PROGRAM ALLOWS UP TO  
THREE DIFFERENT CONSTANT AREA SECTIONS AND ONE TAPERED SECTION  
BETWEEN THE SECOND AND THIRD CONSTANT AREA SECTIONS)  
AREA2 = AREA IN SQ CM OF SECOND CONSTANT AREA SECTION  
AREA3 = AREA IN SQ CM OF THIRD CONSTANT AREA SECTION  
PCONI = POSITION IN CM WHERE FIRST AREA CHANGE OCCURS  
SHPR = PROJECTILE RELEASE PRESSURE IN BARS  
EMPROJ = MASS OF PROJECTILE IN GRAMS



OUTDT1 = DELTA T FOR PRINTING UP TO TIME TMAX1  
TMAX1 = MILLISECS  
OUTDT2 = DELTA T FOR PRINTING UP TO TIME TMAX2  
TMAX2 = MILLISECS  
XSTOP = POSITION IN CM THAT WHEN THE INTERFACE JSTOP REACHES IT,  
THE PROBLEM IS TERMINATED

CARD 9 (7F10.0) REQUIRED ONLY IF INU = 1  
UZERO(I) = INITIAL VELOCITY FOR EACH ZONE

CARD 10 (7F10.0)  
PCON = POSITION IN CM WHERE THIRD AREA CHANGE OCCURS  
SLOPE = SLOPE OF CONSTANT TAPERED SECTION  
RADIUS = RADIUS IN CM OF THE CONSTANT AREA SECTION TO THE RIGHT  
OF THE TAPERED SECTION

CARD 11 (4F10.0I4)  
CALPGM = CALORIES PERGRAM OF POWER  
TBURND = TIME TO BURN POWDER  
GMSPDR = GRAMS OF POWDER  
GASPRS = INITIAL GAS PRESSURE IN POWDER REGION  
IHREL = 0 (NOT APPLICABLE TO GUN PROJECT)





CARD 12 (7F10.0)  
IPIX = 0 ALL PLOTS, ALL PRESSURE POINTS (PLOT ROUTINE MUST BE INCLUDED)  
= 1 ALL PLOTS, NO PRESSURE POINTS  
= 5 NO PLOTS, NO PRESSURE POINTS  
= 6 ONLY PRESSURE POINTS  
NPOX = NUMBER OF PRESSURE POINTS (UP TO FIVE)  
XPO(I) = X POSITION IN CM OF PRESSURE POINT I

CARD 13 (7F10.0) HYPERVELOCITY MODEL LAUNCHER PARAMETERS, (NOT APPLICABLE  
TO GUN PROJECT)  
XPV1 = X POSITION IN CM OF FIRST MEASUREMENT POINT OF PISTON VELOCITY  
XPV2 = X POSITION IN CM OF SECOND MEASUREMENT POINT OF PISTON VELOCITY  
PVERR = PISTON VELOCITY ERROR IN FT PER SEC  
PVMWANT = DESIRED PISTON VELOCITY IN FT PER SEC

CARD 14 (E10.0, 3F10.0)  
R = 8317E 08 GAS CONSTANT  
EMPIST = MASS OF FIRST PISTON SECTION (HYPERVELOCITY MODEL LAUNCHER ONLY)  
FRAC = 1.0  
EMLEAD = MASS OF SECOND PISTON SECTION (HYPERVELOCITY MODEL LAUNCHER)

CARD 15 (7F10.0)  
PO(I) = INITIAL PRESSURE IN PSI IN REGION I

CARD 16 (7F10.0)  
TO(I) = INITIAL TEMPERATURE IN DEGREES KELVIN IN REGION I



CARD 17 (7F10.0)  
AMOL(I) = MOLECULAR WEIGHT OF MATERIAL IN REGION I

CARD 18 (I3)  
ILASTK = 0, STOP  
          = 1, CONTINUE FOR NEW RUN



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